# Optimal Transmission Switching for Reducing Market Power Cost

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## Optimal Transmission Switching for Reducing Market Power Cost

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#### Abstract

The conventional transmission planning tends to focus exclusively on efficiency benefit, allowing cheaper remote generation to have priority dispatch over expensive local generation (least cost approach). Because of this nowadays deregulated markets face the problem that their systems affect the competitiveness of players, giving room for players to exercise market power.

The purpose of this study is to develop a mathematical model that quantifies the generation cost and reduces market power, by minimizing the social cost and restraining producers from withholding generation capacity. To do this, deterministic optimal transmission switching is proposed, together with a Worst-Nash Equilibrium (WNE) optimization, to quantify the social cost.

This study considers the transmission switch formulation based on the DC Optimal Power Flow (DCOPF) presented by Schmuel S. Oren as a Mixed-Integer linear Program (MIP). This formulation employs binary variables to represent the state of the transmission line. The effects of transmission switching with contingency analysis are also considered in the DCOPF formulation.

To include market power cost reduction in our problem, the social cost of the system is modeled considering WNE, which maximizes the social cost using linearization. The formulation includes strategic generators that might choose to withhold some of their output and non-strategic generators. This under the condition that the profit of a portfolio with a strategic generator under Nash Equilibrium is always greater than the profit of a portfolio where the offers are constant.

A 14-node example system is studied where the efficiency benefits and competition benefits of transmission capacity by optimal transmission switching are considered. The results demonstrate that the utilization of the proposed method increase economic benefit and improves competitiveness in the electricity market.

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### Nomenclature

#### Indices

u	generator unit
l	transmission line
i	node of the network
n,m	nodes between line l
k	maximum generation capacity
p	portfolio
s	strategy
С	contingency

#### Sets

U	set of units in the system
L	set of transmission lines in the system
N	set of nodes in the system
K	set of constants
0	set of portfolios in the system
S	set of strategies

#### Model parameters

$c_u$	cost
$\underline{F}$	minimum transmission capacity
$\overline{F}$	maximum transmission capacity
$\overline{g}$	maximum generation capacity
d	demand
В	admitance
$n_c$	operation status of the line during contingency, 0 the line is contingency
	(disconnected)and 1 otherwise
M	arbitrary big number
$\mathbf{C}$	incidence matrix

#### Optimization model variables

SC	social cost
F	power flow in the transmission line
g	generation of each unit
$\widehat{g}$	maximum capacity offer to the market
$n_l$	operation status of the line, 0 the line is disconnected and 1 otherwise
$\pi_p$	profit of portfolio, under Nash equilibrium
$\pi_p^{p,s}$	profit of portfolio, without Nash equilibrium
$\theta$	voltage angle of node $i$
Р	local marginal price at node $i$
x	behavior status of the generating unit, 0 for strategic units
	and 1 for the non-strategic units

- w action of generating unit u, related to the capacity offer to the market
- q quantity produce of an identical product
- ${\cal L}$  Lagrangian optimization function

#### Slackness variables

$ ho_i$	Slackness variable for the energy balance constraint
$\lambda_l^{\rm down}$	Slackness variable for the lower limit of the power flow constraint
$\lambda_l^{\mathrm{up}}$	Slackness variable for the upper limit of the power flow constraint
$\mu_u^{\rm down}$	Slackness variable for the lower limit of the generation limit constraint
$\mu^{\mathrm{up}}_u$	Slackness variable for the upper limit of the generation limit constraint
$\beta_l^{\rm down}$	Slackness variable for the lower limit of the Kirchhoff's law constraint
$\beta_l^{\rm up}$	Slackness variable for the upper limit of the Kirchhoff's law constraint
$\delta_i$	Contingency slackness variable for the energy balance constraint
$\alpha_l^{\rm down}$	Contingency slackness variable for the lower limit of the power flow constraint
$\alpha_l^{\rm up}$	Contingency slackness variable for the upper limit of the power flow constraint
$\varepsilon_l^{\rm down}$	Contingency slackness variable for the lower limit of the Kirchhoff's law constraint
$\varepsilon_l^{\rm up}$	Contingency slackness variable for the upper limit of the Kirchhoff's law constraint

#### Binary variables for Complementary conditions

$b_l^{\mathrm{low}-\lambda}$	Binary variable for the lower limit of the power flow constraint
$b_l^{\mathrm{up}-\lambda}$	Binary variable for the upper limit of the power flow constraint
$b_l^{\mathrm{low}-\mu}$	Binary variable for the lower limit of the generation limit constraint
$b_l^{\mathrm{up}-\mu}$	Binary variable for the upper limit of the generation limit constraint
$b_l^{\mathrm{low}-eta}$	Binary variable for the lower limit of the Kirchhoff's law constraint

 $\begin{array}{ll} b_l^{\mathrm{up}-\beta} & \text{Binary variable for the upper limit of the Kirchhoff's law constraint} \\ b_l^{\mathrm{low}-\alpha} & \text{Contingency binary variable for the lower limit of the power flow constraint} \\ b_l^{\mathrm{up}-\alpha} & \text{Contingency binary variable for the upper limit of the power flow constraint} \\ b_l^{\mathrm{low}-\varepsilon} & \text{Contingency binary variable for the lower limit of the Kirchhoff's law constraint} \\ b_l^{\mathrm{up}-\varepsilon} & \text{Contingency binary variable for the upper limit of the Kirchhoff's law constraint} \end{array}$ 

#### Outputs

F	power flow in the t	ransmission line

- g generation of each unit
- $\widehat{g}$  maximum capacity offer to the market
- $n_l$  operation status of the line, 0 the line is disconnected and 1 otherwise

#### Chapter 1

#### Introduction

#### 1.1 Background

The early electricity industry was designed as vertical integration; where generation, transmission and distribution created a "natural monopoly". This verticalintegrated market led to a lack of incentives to improve the system and reduce generation and distribution costs.

Over the last two decades industry analysts, regulators and policy makers have focused on an economically more efficient system. In December 1996 most of the European electricity markets had changed their policies to achieve a liberalized market, by allowing operating firms to compete freely in the energy market and prevent producers to no longer own the transmission and distribution network [4]. Liberalization decouples generation and transmission sectors; aiming to increase the efficiency, reduce electricity prices and create a more competitive market.

Electricity as a commodity presents special characteristics that must be considered: production must always meet the demand in a short period of time; demand is varying every second; and storage is very limited and expensive [5]. These considerations combined with an inelastic demand, transmission constrains and market fragmentation are incentives for producers to abuse the market equilibrium and alter the electricity price to increase their own profit. This ability of abusing market equilibrium is known as market power.

Market power is one of the main concerns of the deregulated markets nowadays; before liberalization vertical market power was exercised [2], now there is no more concern for that. Instead horizontal market power is a potential problem [6]; when suppliers collude with other suppliers in the market to gain the ability of altering the electricity price.

Evidence of horizontal market power abuse has been observed in several operating electricity markets, where the market price has increased up to 22% above competitive level [7]. Perfect competition price can be set as a benchmark to evaluate market power abuse, different indicators have been studied to quantify market power and its association with cost [8],[1].

There are different forms of market power that can be present; market dominance or local market power (due to transmission congestion). Scholars have studied transmission congestion in the past to recognize the presence of market power in the system [9]. Market dominance concerns strategic producers that are large enough to affect the price and maximize their profit. Strategies as Physical Withholding and Economical Withholding (bids) are implemented to alter the electricity price through horizontal mergers or by collusion. Strategic investment policies can also be implemented to maintain market dominance or increase profit [10].

Physical Withholding or Quantity Withholding occurs when a supplier intentionally decides to offer less generation capacity to the market than its maximum production capacity. Setting market price as the intersection between supply and demand curves [5], the quantity withheld  $(\Delta Q_w)$  makes the supply curve shift to the left and a higher new price is set, increasing it from  $P^*$  to  $P^e$  as in figure (1.1).[1]



Figure 1.1: Withholding strategy and price-quantity outcome [1].

The main consequence of market power exercise is an increase of the generation cost (consequently electricity price) to a higher value than the marginal cost, usually referred to as Market Power Cost [8]. This means an increase of profit for producers and a lower efficiency in the market. The efficiency in the market is measured by its Social Welfare, the summation of producer's surplus and consumer's surplus [2]. The total surplus of the system is the total generation cost minus the variable cost of production. In a perfect competition market, the total surplus reaches its maximum and is considered to be an efficient market. In the case of market power, the social welfare reduces which indicates a lower efficiency. In figure 1.2 an example where in perfect competition the producer generation is 60TWh and its surplus is 6000MSEK, under market power the generating unit can offer less capacity (example 40TWh) until it reaches the maximum surplus of the producer (7000MSEK).



Figure 1.2: Withholding strategy and producers surplus variation [2].

This leads to another important consequence of market power exercise, which is the transfer of wealth from consumers to producers, as shown in figure 1.3. This transfer of wealth under market power directly affects consumers.

In general, perfect competition is assumed in a liberalized market, where no market power is exercised and suppliers bid according to their marginal cost. Nevertheless, in reality, considering the special characteristics of electricity, it is impractical to rely on this assumption. Therefore market power should be considered in the liberalized market and its regulation is of extreme importance to increase efficiency and minimize Social Cost.



Figure 1.3: Transfer of wealth by the exercise of market power [1].

Traditionally, transmission switching analysis is not considered as an economic optimization; most of the studies were based only on system reliability criteria without any economic market analysis, where transmission elements were treated as non-dispatchable elements. Currently there is an agreement to develop a smarter electrical grid which is stronger, more flexible, more efficient and better to control. Optimal transmission switching has proven to be a reliable method of incorporating more controllability to the grid [11], and also creating economic benefit comparing to other methods such as generation unit rescheduling or load shedding [12]. Optimal transmission switching has been complemented with other co-optimizations ancillary services, generation topology and optimal unit commitment scheduling to improve economic efficiency under perfect competition assumption [11],[13].

Under the same assumption in a liberalized electricity market, effective optimal transmission switching has recently proved to be an important tool to improve overall market efficiency and reduce Social Cost [11], [14], [15] considering contingency constraints to prove the system remains stable and robust [16].

Previously market power strategic behavior for economical withholding has being model using Nash-Cournot concepts [17], and physical withholding has being reduce according to demand flexibility [18].

The increase of Social Welfare due to disconnection of a small number of lines in the system has been reported in [19]. Author of [19] suggests that by co-optimizing topology and a simple variation of the network by Transmission System Operators (TSO), market power can be reduced. An impact in market power regulation by transmission augmentation and additional transmission capacity has presented evidence of market power cost by regulating strategic behaviour [20],[21].

In the current electricity market structure, it is important to aim for a more efficient network, a smarter grid that can be more controllable [22]. A fair equilibrium for producers and consumers where there is no transfer of wealth must be procured.

The starting point of this thesis is the work carried out by [14] and [16] to formulate a transmission switching optimization problem to reduce Social Cost, and the work presented by [23] to include Extreme Nash-Equilibria concepts to model the strategic behavior of generating units (Market Power), where linearization techniques are implemented to formulate the problem as a single-stage mixed-integer linear program problem.

This thesis proposes an optimal transmission switching model to minimize Market Power Cost and therefore increase the competition and efficiency in the electricity market and reduce cost for society.

#### 1.2 **Problem Definition**

Perfect competition has been a widely accepted assumption in electricity market studies. However if it is considered that the present deregulated electricity markets affect the competitiveness of players, by big producers being able to exercise market power, the main challenge of the coming environment for electricity market is reducing the cost associated with this behavior.

The idea of this project is to develop a mathematical model in order to: (1) expose how market power can increase social cost by withholding generation capacity, and (2) how optimal network configuration can reduce this cost and increase the competition of players by manipulating the connectivity of the transmission lines.

#### 1.3 Objective

To accomplish this aim, reducing market power cost, two models are studied and integrated. The first model is based on the work made by [14] and [16], that considers traditional schemes of the electricity market with the assumption of perfect competition between players, which is not always the case. To have a better understanding of the real nature of the electricity market, imperfect competition must be included. The second model introduces market power behavior, using Game Theory concepts (Nash equilibrium) to model strategic units in the system, that can choose to withhold capacity offered to the electricity market.

Both models are integrated to have a system under market power conditions where transmission lines can be optimally switched to reduce the market power cost.

#### 1.4 Resources/Tools used

The optimization problem is executed using the General Algebraic Modeling System (GAMS) platform. The deterministic optimization problem is solved with the CPLEX solver in GAMS. The incidence matrices and other sets of parameters are created in MATLAB and transferred to GAMS by using Comma-Separated Values (CSV) files. The code is run on a computer with Intel Xeon E5345 with a 2.33 GHz clocking frequency and 16 GB of RAM. Linear programming relaxation is employed to solve the optimization problem in GAMS.

#### Chapter 2

#### Formulation of the Mathematical Model

Nowadays it is important for the electricity market regulator to minimize any form of market power and to offer the consumer lower cost of generation. This thesis proposes the use of optimal transmission switching by Transmission System Operators to minimize market power behaviour of producers and lower market power cost. To minimize the Social Cost under market power, a DC Optimal Power Flow (DCOPF) model of the system [14] is considered.

This thesis presents an electricity market model that contemplates a market power formulation and a DCOPF formulation with optimal transmission switching, it also includes contingency analysis formulation. Both formulations are integrated in the model as a bi-level optimization problem [24].

This chapter explains the formulation followed to integrate two models. The first assuming perfect competition (DCOPF model) with transmission switching and the second considering market power behavior, based on the substitution of the equations of the DCOPF model by its equivalent optimality conditions, Karush-Kuhn-Tucker (KKT) conditions.

#### 2.1 Assumptions

Following assumptions where made to simplified the model:

- Perfect information;
- No capacity limitations, units have enough installed capacity to supply the load;
- The load is not price sensitive;
- There are no losses in the system,  $\sum_{i=1}^{N} G = \sum_{i=1}^{N} D$ ;
- All lines are available in the initial conditions;
- All generators are available;
- Non-strategic units offer 100% of the maximum capacity to the market;
- Each portfolio (owner) has only one strategic unit;
- Marginal pricing: price is set by the maximum production cost.

#### 2.2 Model Description

A linearized bi-level optimization problem is proposed. First the DC Optimal Power Flow (DCOPF) model (with transmission switching) and Worst-Nash Equilibrium (WNE) model are formulated independently and in detail in section 2.2.1 and section 2.2.2 respectively. Finally the proposed model is formulated in section 2.2.3, integrating the models described in section 2.2.1 and section 2.2.2 as a linearized bi-level optimization using Karush-Kuhn-Tucker (KKT) conditions.

#### 2.2.1 Optimal Transmission Switching

The aim of this model is to minimize the generation cost of the system using optimal transmission switching, subject to physical constraints and Kirchhof laws for power flow. DC approximations are used in the system, so the model can be defined as a linear problem. This model is base under the assumption of perfect competition.

The objective function and constrains of the optimization problem are base on a DC Optimal Power Flow. Objective function and constraints are modified to include the switching of the transmission lines and the cost associated. The objective function of this optimization problem and its constraints are stated below [14]:

Minimize 
$$\sum_{u \in U} c_u g_u + \sum_{l=1}^{L} c_l (1 - n_l)$$
 (2.1a)

Subject to:

$$0 \le g_u \le \overline{g_u} \qquad \qquad \forall u \in U \tag{2.1b}$$

$$\underline{F_l} \ n_l \le F_l \le \overline{F_l} \ n_l \qquad \qquad \forall l \in L \qquad (2.1c)$$

$$g_i + d_i + F_l C_{l,i} = 0 \qquad \qquad \forall i \in N, \forall l \in N \qquad (2.1d)$$

$$B_l \left(\theta_n - \theta_m\right) - F_l + (1 - n_l) M \ge 0 \qquad \forall l \in L \qquad (2.1e)$$

$$B_l \left(\theta_n - \theta_m\right) - F_l - \left(1 - n_l\right) M \le 0 \qquad \qquad \forall l \in L \qquad (2.1f)$$

This formulation includes a new element:  $n_l$ , which is a binary variable, and it represents the connection status of each transmission line in the system. When a line l is connected,  $n_l = 1$  and when it has been removed or opened,  $n_l = 0$ . The objective function (2.1a) includes the cost of switching a transmission line. The constraints of the optimization problem are:

- The generation limits of each unit (2.1b);
- The power flow limits of the line (2.1c). All lines are modelled with the same maximum transmission capacity. The binary variable  $n_l$  enables the maximum capacity of the line when the line is connected and limits it to zero when the line is disconnected.
- The energy balance constraint (2.1d).
- Kirchhoff's law (2.1e),(2.1f), the mathematical function of this two equation is to accentuate the fact that a disconnected line has no power flow. If the line is connected, this variable will be zero and the formula represents the connection of the line between nodes n and m. The parameter M is an arbitrary large number, and it is introduced to influence how the system perceives the network configuration. If a transmission line is connected (nl=1) Kirchhoff Law represents the connection of the line between the nodes and the angles difference between  $\theta_m$  and  $\theta_n$  will encourage the power flow through the line. When the line is disconnected (nl=0) these two equations will no longer represent this angle difference between nodes (only a numerical affirmation) and completes the formulation to represent the disconnection of the line. This formulation will ensure no flow in an opened line [14].

#### **Contingency Analysis**

To ensure the system is able to sustain its reliability, contingency analysis is considered in the formulation. Additional constrains are added to the previous (2.1) to include the contingency status of the system:

$$\underline{F_{lc}} n_l n_c \le F_{lc} \le F_{lc} n_l n_c \qquad \forall l \in_L$$
(2.2a)

$$g_i + d_i + F_{lc}C_{l,i} = 0 \qquad \qquad \forall i \in N, \forall l \in N \qquad (2.2b)$$

$$B_l \left(\theta_{nc} - \theta_{mc}\right) - F_{lc} + \left(2 - n_l - n_c\right) M \ge 0 \qquad \forall l \in_L$$

$$(2.2c)$$

$$B_l \left(\theta_{nc} - \theta_{mc}\right) - F_{lc} - \left(2 - n_l - n_c\right) M \le 0 \qquad \forall l \in_L$$

$$(2.2d)$$

A new element  $n_c$  (binary variable) is included in this constraints (2.2) to represent the connection status of each transmission line in the system during contingency [16]. Contingency is defined as the loss of one single element in the system, in this case a transmission line. When line l is contingency,  $n_c = 0$  (for line l) and when is not contingency,  $n_c = 1$ .

Equations (2.1)-(2.2) formulate the model for DCOPF with Optimal Transmission Switching (OTS) and Contingency Analysis.

#### 2.2.2 Worst-Nash Equilibrium

Assuming that generating units can behave strategically, choosing to withhold some of their outputs, we consider that market power is exercised by a supplier (owner of a strategic unit) when it is intentionally withholding its production capacity. This action will increase the cost of generation in the system and increase the profit of the unit. Perfect competition conditions for electricity market studies, where all units are non-strategic units (are assumed to bid competitively) is no longer an assumption, since some units are considered to be strategic in this model.

Game theory concepts are used in this project to model the strategic decision of the generating units, in particular Cournot Competition and Nash Equilibrium concepts.

The Cournot Competition concepts considered for this project include: (1) Few players (suppliers) and many strategies. (2) Strategies are define as the quantities (q) the players produce of an identical product. (3) The cost of production is  $c_u q$  (with a constant marginal cost). (4) Players aime to maximize their profit [25].

A strategy profile  $S_p$  is a Nash Equilibrium if for each individual player, its choice s is the best response to the other players choices. Figure 2.1 shows the response curve of two players; BR1(R2) reflects the best responses of player 1 (R1) according to player 2 responses (R2), the same for BR2(R1). The strategy chosen by the each player where they intersect ( $R1^*$  and  $R2^*$  respectively) is the the Nash Equilibrium response for each of them.

Some considerations under Nash Equilibrium are: (1) Under Nash Equilibrium there is no individual incentive of each player to deviate from s if all actions of all players are hold constant. Only under Nash Equilibrium are no regrets for all players. (2) Everybody in the game believes that everybody else will also play their particular part in the Nash Equilibrium. (3) There can be many Nash Equilibriums for a problem. Problems can converge to a bad equilibrium for players base on decreasing the profits, and can also converge to a good equilibrium for the players base on increasing profits [26], [27].



Figure 2.1: Nash equilibrium found by two players [3].

When all players reach their own strategy and thereby have maximized their own profit ( $\pi_p$ ), the Nash Equilibrium has been reached [28]. In this study suppliers (producers) will act as players trying to find the Nash equilibrium to maximize their profit. Market power in the system is model as the Worst-Nash Equilibrium (WNE), defined as the Nash Equilibrium which maximizes the generation cost (Social Cost).

There will be strategic units and non-strategic units in the formulation. For this model, each producer that owns an strategic unit is define as to posses a portfolio for each strategic unit it owns. For simplicity it is assumed that each owner that behaves strategically may have maximum one portfolio. Then there will be as many portfolios as strategic units are. Where the strategic unit is able to exercise strategies considering Nash equilibrium.

The aim of this model (2.3) is to maximize the generation cost (Social Cost) of the system an obtain the Worst-Nash Equilibrium, subjected to the two main constraints. These constraints are:

- Non-strategic units will offer their maximum capacity to the system and strategic units can choose from a finite set of actions how much they will offer to the market.
- The profit of a portfolio under Nash Equilibria  $(\pi_p)$  is higher than the profit of a portfolio that does not considers Nash Equilibria for its dispatch  $(\pi_p^{p,s})$ .

Maximize 
$$\sum_{u \in U} c_u g_u$$
 (2.3a)

Subject to:

$$\widehat{g}_u = \sum_{k=1}^{K} \overline{g}_u x_{uk} w_k + w_0 \overline{g}_u \qquad \forall u \in U$$
(2.3b)

$$\pi_p \ge \pi_p^{p,s} \qquad \qquad u \in U \tag{2.3c}$$

Strategic and non-strategic units u are part of the set of generating units U, have a variable cost of production  $c_u$  and their production under Nash Equilibrium is  $g_u$ . Then the generation cost or Social Cost (SC) under Nash Equilibrium is define (2.3a). The offered capacity ( $\hat{g}_u$ ) of a strategic unit is determined by profit maximization. In (2.3b)  $\bar{g}_u$  is the maximum capacity of the generating unit u, the binary variable  $x_{uk}$  indicates whether the unit is strategic  $x_{uk} = 0$  or nonstrategic  $x_{uk} = 1$ . The percentage of maximum capacity that a strategic unit will offer is defined by  $w_0$ . And the withheld capacity is defined by  $w_k$  so that  $\sum_{k=1}^{K} w_k = 1 - w_0$ . So when the unit is non-strategic  $\sum_{k=0}^{K} w_k = 1$  and the unit will offer its maximum capacity (2.4). Each strategic unit is assumed to have potentially 4 levels of output, therefore each portfolio will have 4 different possible strategies; since a portfolio has only one strategic unit and no non-strategic units.

$$\widehat{g}_{u} = \begin{cases} \overline{g}_{u}w_{0} & \text{if } x_{uk} = 0\\ \overline{g}_{u}\sum_{k=0}^{K} w_{k} & \text{if } x_{uk} = 1 \end{cases}$$

$$(2.4)$$

It is stated before and again in (2.3c) that the profit of a portfolio under Nash Equilibrium  $\pi_u$  is greater than the profit of the same portfolio rather than when it is not considering the equilibrium strategies  $(\pi_p^{p,s})$ . We said that the same portfolio does not considers Nash equilibrium when we hold the offers of every other portfolio constant, and replace the offer of this portfolio with another strategic combination  $s \in S_p$  [28]. If there were more than one strategic unit for portfolio, the profit of it would be the sum of the individual profits of each strategic units  $(\pi_u)$  as:

$$\pi_p = \sum_{u \in O(p)} \pi_u$$

For the proposed model the profit of a portfolio p,  $\pi_p$ , is the same as the profit of a unit u,  $\pi_u$ . The profit of a single unit can be defined as:  $\pi_u = (P_i - c_u)g_u$ , where  $P_i$  is the local marginal price at the node *i*,  $c_u$  is the variable cost of the unit and  $g_u$  is its respectively dispatch. This equation can also be expressed as  $\pi_u = \mu_u^{up} \hat{g}_u$ , where  $\mu_u^{up}$  is the Lagrange multiplier of the constraint of each unit so it cannot exceed its offer.

The expression for the profit of a unit  $\pi_u$  is not linear, so to linearize this expression two considerations are made [23]:

(1) If X and Y are positive variables in an optimization problem, b is a binary variable and M is a large number, the non-linear equation XY = 0 can be rewritten:

$$X_b + Y(1-b) = 0 (2.5a)$$

Can be written as two simple linear constrains:

$$-M(1-b) \le X \le M(1-b)$$
 (2.5b)

$$-Mb \le Y \le Mb \tag{2.5c}$$

(2) Considering if  $\lambda$  is a Lagrange multiplier and x is a decision variable, the multiplication of this two variables is not linear, supposing that x takes a set of finite values  $x = \sum_{j=1}^{m} a_j b_j + a_0$  for constants  $a_0, ..., a_m$  and m binary variables  $b_1, ..., b_m$ . Introducing a new variable  $c_j$  that satisfies:  $c_j - \lambda b_j = 0$ . This expression is of the form of (2.5a) and can be written as two simple linear constraints (2.5b),(2.5c).

Then the expression for the profit of a unit  $\pi_u$  is linearize introducing a variable  $z_{uk} = \mu_u^{up} x_{uk}$ , where  $x_{uk}$  is a binary variable. The equation  $z_{uk}$  is now linearized as three equations [23]:

$$z_{uk} - \mu_u^{\text{up}} \le M \left( 1 - x_{uk} \right) \tag{2.6a}$$

$$z_{uk} - \mu_u^{up} \ge -M (1 - x_{uk})$$
 (2.6b)

$$z_{uk} \le M x_{uk} \tag{2.6c}$$

Introducing linearized equations (2.6) to the definition of the profit of a portfolio  $\pi_p$ :

$$\pi_p = \sum_{k=1}^{K} k_u z_{uk} w_k + \mu_u^{up} w_0 k u$$
(2.7)

The model to obtain the Worst-Nash Equilibrium is formulated in (2.3)-(2.7). These equations are linearized, so the model can be defined as a linear problem.

#### 2.2.3 Integrated Model of Optimal Transmission Switching and Worst-Nash Equilibrium

Nowadays it is important for the electricity market regulator to minimize any form of market power and to offer the consumers lower cost of generation. This thesis proposes the use of optimal transmission switching implemented by Transmission System Operators to minimize market power behaviour of producers and lower market power cost. A linearized bi-level optimization problem is proposed, WNE formulation and OTS formulation are integrated as a set of primary conditions and secondary conditions respectively. This integration is based on the substitution of the OTS formulation by its equivalent optimal conditions, also known as Karush-Kuhn-Tucker (KKT) conditions [29],[30]. The primary conditions are defined by the same formulation presented for the WNE model (2.3)-(2.7).

KKT conditions are developed for the DCOPF with Optimal Transmission Switching and Contingency Analysis model, these conditions will be defined as the secondary conditions of our integrated model. The inner dispatch problem minimizes the social cost, subject to constrains as in (2.1)-(2.2), except for (2.1b) which from now on will be redefine as  $0 \le g_u \le \widehat{g_u}$  (2.8b) to include the strategic units behavior. The secondary conditions are defined as:

Maximize 
$$-\sum_{u \in U} c_u g_u + \sum_{l=1}^{L} c_l (1 - n_l)$$
 (2.8a)

Subject to:

$$0 \le g_u \le \widehat{g_u} \qquad \qquad \forall u \in U \qquad (2.8b)$$

$$\underline{F_l} \ n_l \le F_l \le F_l \ n_l \qquad \qquad \forall l \in L \qquad (2.8c)$$

$$g_i + d_i + F_l C_{l,i} = 0 \qquad \qquad \forall i \in N \tag{2.8d}$$

$$B_l(\theta_n - \theta_m) - F_l + (1 - n_l) M \ge 0 \qquad \forall l \in L \qquad (2.8e)$$

$$B_l(\theta_n - \theta_m) - F_l - (1 - n_l)M \le 0 \qquad \forall l \in L \qquad (2.8f)$$

$$\underline{F_{lc}} n_l n_c \le F_{lc} \le F_{lc} n_l n_c \qquad \forall l \in L \qquad (2.8g)$$

$$g_i + d_i + F_{lc}C_{l,i} = 0 \qquad \qquad \forall i \in N \tag{2.8h}$$

$$B_l \left(\theta_{nc} - \theta_{mc}\right) - F_{lc} + \left(2 - n_l - n_c\right) M \ge 0 \qquad \forall l \in L \qquad (2.8i)$$

$$B_l \left(\theta_{nc} - \theta_{mc}\right) - F_{lc} - \left(2 - n_l - n_c\right) M \le 0 \qquad \forall l \in L \qquad (2.8j)$$

First the Lagrangian function of the DCOPF with Optimal Transmission Switching and Contingency Analysis of (2.8) is defined as (2.9). Where  $\rho_i$ ,  $\lambda_l^{\text{down}}$ ,  $\lambda_l^{\text{up}}$ ,  $\mu_u^{\text{down}}$ ,  $\mu_u^{\text{up}}$ ,  $\beta_l^{\text{down}}$ ,  $\beta_l^{\text{up}}$ ,  $\delta_i$ ,  $\alpha_l^{\text{down}}$ ,  $\alpha_l^{\text{up}}$ ,  $\varepsilon_l^{\text{down}}$  and  $\varepsilon_l^{\text{up}}$  are the Lagrange multipliers of the problem constraints.

$$\begin{aligned} \mathcal{L} &= -\sum_{u \in U} c_u g_u + \sum_{l=1}^{L} c_l (1 - n_l) \\ &+ \rho_i \left( g_i + d_i + F_l C_{l,i} \right) \\ &+ \sum_{l=1}^{L} \lambda_l^{\text{down}} \left( \underline{F_l} \ n_l - F_l \right) + \sum_{l=1}^{L} \lambda_l^{\text{up}} \left( F_l - \overline{F_l} \ n_l \right) \\ &+ \sum_{u}^{U} \mu_u^{\text{down}} \left( \underline{g_u} - g_u \right) + \sum_{u}^{U} \mu_u^{\text{up}} \left( g_u - \overline{g_u} \right) \\ &+ \sum_{l=1}^{L} \beta_l^{\text{down}} \left( -B_l \left( \theta_n - \theta_m \right) + F_l - (1 - n_l) M \right) \\ &+ \sum_{l=1}^{L} \beta_l^{\text{up}} \left( B_l \left( \theta_n - \theta_m \right) - F_l - (1 - n_l) M \right) \\ &+ \delta_i \left( g_i + d_i + F_{lc} C_{l,i} \right) \\ &+ \sum_{l=1}^{L} \alpha_l^{\text{down}} \left( \underline{F_{lc}} \ n_l \ n_c - F_{lc} \right) \\ &+ \sum_{l=1}^{L} \varepsilon_l^{\text{down}} \left( -B_l \left( \theta_{nc} - \theta_{mc} \right) + F_{lc} - (2 - n_l - n_c) M \right) \end{aligned}$$

$$(2.9)$$

The Dual feasibility conditions are:

$$\rho_i, \delta_i \to \text{free} \qquad \forall_i \in N \qquad (2.10a)$$

$$\lambda_l^{\text{down}}, \lambda_l^{\text{up}} \ge 0 \qquad \qquad \forall_l \in L \qquad (2.10b)$$

$\mu_u^{\text{down}}, \mu_u^{\text{up}} \ge 0$	$\forall_u \in U$	(2.10c)
$\beta_l^{\rm down},\beta_l^{\rm up}\geq 0$	$\forall_l \in L$	(2.10d)
$\alpha_l^{\rm down}, \alpha_l^{\rm up} \geq 0$	$\forall_l \in L$	(2.10e)
$\varepsilon_l^{\rm down}, \varepsilon_l^{\rm up} \geq 0$	$\forall_l \in L$	(2.10f)

The Lagrangian function is formulated by setting each side of the constraints less/equal to zero, separating the lower boundary from the upper boundary conditions. Each of this conditions are multiplied by a Lagrange multiplier respectively. Finally, the objective function is added to the sum of these constraints as in (2.9).

The process is known as Lagrange relaxation, where these changes an unconstrain problem of minimization is obtain from a constrain problem with equality and inequality restrictions [29]. Now KKT conditions are derive from the Lagrangian.

The stationary conditions derived from the Lagrangian are defined as:

$$\frac{\partial \mathcal{L}}{\partial g_u} = -c_u + \rho_i - \mu_u^{\text{down}} + \mu_u^{\text{up}} + \delta_i = 0$$
(2.11a)

$$\frac{\partial \mathcal{L}}{\partial \theta_i} = \sum_{l=1}^{L} \beta_l^{\text{down}} \left( C_{i,l} \right)^T B_l - \sum_{l=1}^{L} \beta_l^{\text{up}} \left( C_{i,l} \right)^T B_l = 0$$
(2.11b)

$$\frac{\partial \mathcal{L}}{\partial F_l} = \rho_i - \lambda_l^{\text{down}} + \lambda_l^{\text{up}} + \beta_l^{\text{down}} - \beta_l^{\text{up}} = 0$$
(2.11c)

$$\frac{\partial \mathcal{L}}{\partial \theta_{ic}} = \sum_{l=1}^{L} \varepsilon_l^{\text{down}} \left( C_{i,l} \right)^T B_l - \sum_{l=1}^{L} \varepsilon_l^{\text{up}} \left( C_{i,l} \right)^T B_l = 0$$
(2.11d)

$$\frac{\partial \mathcal{L}}{\partial F_{lc}} = \delta_i - \alpha_l^{\text{down}} + \alpha_l^{\text{up}} + \varepsilon_l^{\text{down}} - \varepsilon_l^{\text{up}} = 0$$
(2.11e)

The stationary conditions (2.11) are defined as the partial derivatives of the Lagrange function in respect to the variables of the secondary conditions and equal
to zero. These variables are  $g_u$ ,  $\theta_i$ ,  $F_l$ ,  $\theta_{ic}$  and  $F_{lc}$ .

Then complementary slackness conditions derived from the Lagrange function:

$$\sum_{l=1}^{L} \lambda_l^{\text{down}} \left( \underline{F_l} \ n_l - F_l \right) = 0 \qquad \forall l \in L \qquad (2.12a)$$

$$\sum_{\substack{l=1\\U}}^{L} \lambda_l^{\text{up}} \left( F_l - \overline{F_l} \ n_l \right) = 0 \qquad \forall l \in L \qquad (2.12b)$$

$$\sum_{u}^{U} \mu_{u}^{\text{down}} \left( \underline{g_{u}} - g_{u} \right) = 0 \qquad \qquad \forall u \in U \qquad (2.12c)$$

$$\sum_{u}^{U} \mu_{u}^{\mathrm{up}} \left( g_{u} - \overline{g_{u}} \right) = 0 \qquad \qquad \forall u \in U \qquad (2.12\mathrm{d})$$

$$\sum_{l=1}^{L} \beta_l^{\text{down}} \left( -B_l \left( \theta_n - \theta_m \right) + F_l - (1 - n_l) M \right) = 0 \qquad \forall l \in L \qquad (2.12e)$$

$$\sum_{l=1}^{L} \beta_l^{\mathrm{up}} \Big( B_l \left( \theta_n - \theta_m \right) - F_l - (1 - n_l) M \Big) = 0 \qquad \forall l \in L \qquad (2.12f)$$

$$\sum_{l=1}^{L} \alpha_l^{\text{down}} \left( \underline{F_{lc}} \ n_l \ n_c - F_{lc} \right) = 0 \qquad \forall l \in L \qquad (2.12g)$$

$$\sum_{l=1}^{L} \alpha_l^{\rm up} \Big( F_{lc} - \overline{F_{lc}} \ n_l \ n_c \Big) = 0 \qquad \qquad \forall l \in L \qquad (2.12h)$$

$$\sum_{l=1}^{L} \varepsilon_l^{\text{down}} \left( -B_l \left( \theta_{nc} - \theta_{mc} \right) + F_{lc} - \left( 2 - n_l - n_c \right) M \right) = 0 \qquad \forall l \in L \qquad (2.12i)$$

$$\sum_{l=1}^{L} \varepsilon_l^{\text{up}} \Big( B_l \left( \theta_{nc} - \theta_{mc} \right) - F_{lc} - \left( 2 - n_l - n_c \right) M \Big) = 0 \qquad \forall l \in L \qquad (2.12j)$$

These complementary conditions only consider the constraints that are defined as less/equal than zero. They are the lower boundary and upper boundary of each constrain multiplied by their respective Lagrange multiplier and equal to zero. Conditions in (2.12) are no-linear. To guaranty that the KKT conditions solve the problem and obtain the global optimal solution, these equations are reformulated as a Mix Integer Linear Programming problem (MILP) by introducing binary variables to linearize the problem as was estate above in (2.5). A set of two linear linear equations represent each equation of the complementary slackness condition:

$$-M\left(1-b_{l}^{\mathrm{low}-\lambda}\right) \leq \left(\underline{F_{l}} \ n_{l}-F_{l}\right) \leq M\left(1-b_{l}^{\mathrm{low}-\lambda}\right)$$
(2.13a)

$$-M\left(b_{l}^{\mathrm{low}-\lambda}\right) \leq \lambda_{l}^{\mathrm{low}} \leq M\left(b_{l}^{\mathrm{low}-\lambda}\right)$$
(2.13b)

$$-M\left(1-b_l^{\mathrm{up}-\lambda}\right) \le \left(F_l - \overline{F_l} \ n_l\right) \le M\left(1-b_l^{\mathrm{up}-\lambda}\right)$$
(2.13c)

$$-M\left(b_{l}^{\mathrm{up}-\lambda}\right) \leq \lambda_{l}^{\mathrm{up}} \leq M\left(b_{l}^{\mathrm{up}-\lambda}\right)$$

$$(2.13d)$$

$$-M\left(1-b_{u}^{\mathrm{low}-\mu}\right) \leq \left(\underline{g_{u}}-g_{u}\right) \leq M\left(1-b_{u}^{\mathrm{low}-\mu}\right)$$
(2.13e)

$$-M\left(b_{u}^{\mathrm{low}-\mu}\right) \leq \mu_{u}^{\mathrm{low}} \leq M\left(b_{u}^{\mathrm{low}-\mu}\right)$$
(2.13f)

$$-M\left(1-b_{u}^{\mathrm{up}-\mu}\right) \leq \left(g_{u}-\overline{g_{u}}\right) \leq M\left(1-b_{u}^{\mathrm{up}-\mu}\right)$$

$$(2.13g)$$

$$-M\left(b_{u}^{\mathrm{up}-\mu}\right) \leq \mu_{u}^{\mathrm{up}} \leq M\left(b_{u}^{\mathrm{up}-\mu}\right)$$

$$(2.13h)$$

$$-M\left(1-b_{l}^{\mathrm{low}-\beta}\right) \leq \left(-B_{l}\left(\theta_{n}-\theta_{m}\right)+F_{l}-\left(1-n_{l}\right)M\right) \leq M\left(1-b_{l}^{\mathrm{low}-\beta}\right)$$
(2.13i)

$$-M\left(b_{l}^{\mathrm{low}-\beta}\right) \leq \beta_{l}^{\mathrm{low}} \leq M\left(b_{l}^{\mathrm{low}-\beta}\right)$$
(2.13j)

$$-M\left(1-b_l^{\mathrm{up}-\beta}\right) \le \left(B_l\left(\theta_n-\theta_m\right)-F_l-\left(1-n_l\right)M\right) \le M\left(1-b_l^{\mathrm{up}-\beta}\right) \quad (2.13\mathrm{k})$$

$$-M\left(b_{l}^{\mathrm{up}-\beta}\right) \leq \beta_{l}^{\mathrm{up}} \leq M\left(b_{l}^{\mathrm{up}-\beta}\right)$$

$$(2.131)$$

$$-M\left(1-b_{l}^{\mathrm{low}-\alpha}\right) \leq \left(\underline{F_{lc}} \ n_{l} \ n_{c} - F_{lc}\right) \leq M\left(1-b_{l}^{\mathrm{low}-\alpha}\right)$$
(2.13m)

$$-M\left(b_{l}^{\mathrm{low}-\alpha}\right) \leq \alpha_{l}^{\mathrm{low}} \leq M\left(b_{l}^{\mathrm{low}-\alpha}\right)$$
(2.13n)

$$-M\left(1-b_l^{\mathrm{up}-\alpha}\right) \le \left(F_{lc}-\overline{F_{lc}} \ n_l \ n_c\right) \le M\left(1-b_l^{\mathrm{up}-\alpha}\right)$$
(2.130)

$$-M\left(b_{l}^{\mathrm{up}-\alpha}\right) \leq \alpha_{l}^{\mathrm{up}} \leq M\left(b_{l}^{\mathrm{up}-\alpha}\right)$$

$$(2.13p)$$

$$-M\left(1-b_{l}^{\mathrm{low}-\varepsilon}\right) \leq \left(-B_{l}\left(\theta_{nc}-\theta_{mc}\right)+F_{lc}-\left(2-n_{l}-n_{c}\right)M\right) \leq M\left(1-b_{l}^{\mathrm{low}-\varepsilon}\right)$$

$$(2.13q)$$

$$-M\left(b_{l}^{\mathrm{low}-\varepsilon}\right) \leq \varepsilon_{l}^{\mathrm{low}} \leq M\left(b_{l}^{\mathrm{low}-\varepsilon}\right)$$
(2.13r)

$$-M\left(1-b_{l}^{\mathrm{up}-\varepsilon}\right) \leq \left(B_{l}\left(\theta_{nc}-\theta_{mc}\right)-F_{lc}-\left(2-n_{l}-n_{c}\right)M\right) \leq M\left(1-b_{l}^{\mathrm{up}-\varepsilon}\right)$$

$$(2.13s)$$

$$-M\left(b_{l}^{\mathrm{up}-\varepsilon}\right) \leq \varepsilon_{l}^{\mathrm{up}} \leq M\left(b_{l}^{\mathrm{up}-\varepsilon}\right)$$

$$(2.13t)$$

Recalling that the primary conditions are defined by the same formulation presented for the WNE model (2.3)-(2.7), the integration of the secondary conditions to the primary conditions in the bi-level problem is now complete by defining the secondary conditions as (2.8), (2.11) and (2.13).

The complete optimization problem is formulated in (2.14), where the objective function is to find the the maximum Social Cost under Nash equilibrium and minimize it by implementing Optimal Transmission Switching. The overall problem is a Mixed-Integer Linear Program:

Maximize	(2.8a)	(2.14a)
Subject to:	(2.3b) - (2.7), (2.8b) - (2.8j), (2.11), (2.13)	
		(2.14b)

### Chapter 3

### IEEE 14 Bus Test Case, Results and Discussion

For a better understanding the IEEE fourteen node example system is modified and used to illustrate the proposed model. Data from the system was obtained from the University of Washington Power System Test Case Archive [31]. Both transmission switching in perfect competition and under market power are applied to the modified IEEE 14-node example system and studied in detail. The deterministic optimization problem is solved with the CPLEX solver in General Algebraic Modeling System (GAMS) platform [32]. The incidence matrices and other sets of parameters are created in MATLAB and transferred to GAMS by using Coma-Separated Values (CSV) files. The code is run on a computer with Intel Xeon E5345 with a 2.33 GHz clocking frequency and 16 GB of RAM. Linear programming relaxation is employed to solve the optimization problem in GAMS.

### 3.1 Modified IEEE 14 Node Example System

The modified IEEE 14-node example system is illustrated in figure 3.1, this example system has fourteen nodes and twenty power lines. The generation costs are assumed to be linear, resistance of the line and shunt capacitance are zero, maximum transmission capacity of the lines is set to 20MW, losses and reactive power are ignored. The example system in figure 3.1 is modified to have three portfolios, each with one strategic unit that has four possible levels of output. The strategic units are  $u_3$ ,  $u_5$  and  $u_6$  (shadow units) and they belong to Portfolio 1, Portfolio 2 and Portfolio 3 respectively. The characteristics of the generators is presented in table 3.1, table 3.2 shows the load data and transmission lines data is presented in table 3.3. Modifications from the IEEE test system are made for the generators data, also synchronous condensers (bus 3, bus 6 and bus 8) are not considered for this study.

ID	Bus	Unit Size [MW]	Cost of generation [\$/MWh]
$u_1$	1	30	30
$u_2$	2	200	20
$u_3$	3	150	100
$u_4$	3	100	10000
$u_5$	13	100	5000
$u_6$	6	100	100
$u_7$	3	100	150
$u_8$	14	100	100

Table 3.1: Generator data.

### 3.2 Results and Discussion

## 3.2.1 The Traditional Model for Perfect Competition vs. Nash Equilibria Model

The traditional model for perfect competition is a Mixed Integer Linear Programming problem presented in (2.1) as Optimal Power Flow formulation, coded using



Figure 3.1: Single line diagram of the 14 node example system.

the GAMS platform and solved with the CPLEX solver. The optimal generation dispatch for the 14-node example system in perfect competition is shown in table 3.4. Transmission switching under perfect competition (A transmission element open) will result in SC increase, therefor the optimal solution is no transmission element open (minimum SC). When Nash equilibrium is considered in the example system with no transmission switching in the lines, the results are referred to as Base Case study. The MILP programming dispatch results are obtained and

Bus	Total Demand [MW]	
2	21.7	
3	94.2	
4	47.8	
5	7.6	
6	11.2	
9	29.5	
10	9	
11	3.5	
12	6.1	
13	13.5	
14	14.9	

Table 3.2: Load data.

presented in table 3.5.

Under traditional perfect competition,  $u_3$  offers its true marginal cost to the market. The same unit under Nash equilibrium withholds about 93.75% of its real capacity. The Base Case where units are allowed to have strategic behavior by withholding capacity, shows a drastic increase in social cost from \$20688 MWh to \$60117 MWh, which is almost 290%.

This study shows the impact that strategically behaving generators can cause and how important it is to control its disposition to physical withholding. It also provides with a better understanding of how important it is to consider market power when economic considerations are studied in the system and social cost is to be minimized.

ID	From Bus	To Bus	$X_{\rm ID} \left[\Omega\right]$
$L_1$	1	2	0.05917
$L_2$	1	5	0.22304
$L_3$	2	3	0.19797
$L_4$	2	4	0.17632
$L_5$	2	5	0.17388
$L_6$	3	4	0.17103
$L_7$	4	5	0.04211
$L_8$	4	7	0.20912
$L_9$	4	9	0.55618
$L_{10}$	5	6	0.25202
$L_{11}$	6	11	0.19890
$L_{12}$	6	12	0.25581
$L_{13}$	6	13	0.13027
$L_{14}$	7	8	0.17615
$L_{15}$	7	9	0.11001
$L_{16}$	9	10	0.08450
$L_{17}$	9	14	0.27038
$L_{18}$	10	11	0.19207
$L_{19}$	12	13	0.19988
$L_{20}$	13	14	0.34802

Table 3.3: Line data.

### 3.2.2 The Proposed Model for Reducing Market Power Cost

In contrast with the Base Case for the Nash Equilibrium model, the proposed model for reducing market power cost (2.14) applied to the 14-node example system can be used to obtain an optimal planning for switching several lines in the system (lines 4-9 and 13-14). After opening the transmission lines suggested by the program, the system's network is shown as in figure 3.2.

u	$g \; [\mathrm{MW}]$	Cost $[\/h]$
$u_1$	30	900
$u_2$	38.89	777.8
$u_3$	101.762	10176.2
$u_4$	0	0
$u_5$	0	0
$u_6$	46.828	4682.8
$u_7$	0	0
$u_8$	41.52	4152
Total	259	20689

Table 3.4: Optimal dispatch for perfect competition.

Table 3.5: Optimal dispatch under Nash equilibrium (base case).

u	$g \; [\mathrm{MW}]$	Cost $[$/h]$
$u_1$	30	900
$u_2$	44.441	888.82
$u_3$	9.375	937.5
$u_4$	2.203	22030
$u_5$	2.666	13330
$u_6$	25	2500
$u_7$	100	15000
$u_8$	45.316	4531.6
Total	259	60118

u	$g \; [MW]$	Cost $[\$/h]$
$u_1$	0.0007	0.021
$u_2$	101.699	2033.98
$u_3$	84	8400
$u_4$	0	0
$u_5$	0	0
$u_6$	38.4	3840
$u_7$	0	0
$u_8$	34.9	3490
Total	259	17764

Table 3.6: Optimal dispatch under Nash equilibrium (switched line).

Table 3.7: Generation capacity offer to the market in the base case.

u	$\overline{g}$ [MW]	$\widehat{g}$ [MW]
$u_1$	30	30
$u_2$	200	200
$u_3$	150	84
$u_4$	100	100
$u_5$	100	32.15
$u_6$	100	38.4
$u_7$	100	100
$u_8$	100	100

The new topology of the system changes the power flow of the lines as shown in table 3.8. It shows an increase of 233.3% in congested lines. When a fault occurs in one of the transmission lines that are congested before switching, the proposed model shows the system remains stable and transmission lines are optimally switched off to minimize the social cost.

The results show a significantly lower Social Cost compared to the Base Case,

	$F_L$ [MW]	
ID	Before	After
$L_1$	14.199	-19.9
$L_2$	15.801	20
$L_3$	1.502	20
$L_4$	20	20
$L_5$	15.437	20
$L_6$	18.88	9.8
$L_7$	20	20
$L_8$	7.04	-
$L_9$	4.04	2
$L_{10}$	3.638	12.4
$L_{11}$	10.92	20
$L_{12}$	3.53	3.525
$L_{13}$	2.988	16.075
$L_{14}$	0	0
$L_{15}$	7.04	-
$L_{16}$	12.5	12.5
$L_{17}$	-20	-20
$L_{18}$	-3.5	-3.5
$L_{19}$	-2.57	-2.575
$L_{20}$	10.416	-

Table 3.8: Power flow before/after switching.



Figure 3.2: Single line diagram of the 14 node example system after switching.

table 3.9, with a reduction of 70.45%. This proposed model encourages strategic units  $(u_3, u_5, u_6)$  to be more competitive and offer more capacity to the market, as it is shown in table 3.10. Hereby the total withheld capacity of the system has been reduced from 70.4% to 55.8% (figure 3.3) of the installed capacity in strategic generators, which is an increase of 51.43MW capacity offered to the market. The strategic units  $u_3$  and  $u_6$  are the major contributors to reducing the Social Cost by

# lines switched	Open Lines	SC [\$/MWh]
0	-	60118
2	Bus 4-9, Bus 13-14	17764

Table 3.9: Social cost.

Table 3.10: Generation capacity offer before/after switching.

u	$\overline{g}$ [MW]	$\widehat{g}_u$ [MW]	
		before	after
$u_1$	30	30	30
$u_2$	200	200	200
$u_3$	150	9.375	84
$u_4$	100	100	100
$u_5$	100	68.75	32.15
$u_6$	100	25	38.4
$u_7$	100	100	100
$u_8$	100	100	100

clearly reducing their withheld strategy, bidding more competitively and offering a capacity closer to their maximum as is shown in figure 3.4 and figure 3.5.

Optimal Transmission Switching reduces the total withholding, but looking closely at table 3.10 we can see that  $u_5$  instead of reducing its own withholding, the proposed model has given it incentive to exercise more market power (figure 3.6); nevertheless the total Social Cost still decreases and hence society benefits from it.

The switching of these lines (lines 4-9 and 13-14) jointly give the highest social cost reduction. If there is a limitation on the number of lines that are allowed to switch and it is lower than the optimal solution, the Social Cost will still be reduced and lower than the Base Case social cost, but will be higher than the



Figure 3.3: Impact of optimal transmission switching in withholding reduction.

optimal solution.

It has been proven that Optimal Transmission Switching can be used as one of many policies to increase Competition Benefit by minimizing market power cost. These results show the high impact of switching a small number of lines in the system on the total operational cost. It is important to notice that the proposed method is made for the systems that were designed or expanded by only taking into consideration the excess demand in the system, therefore the Social Cost are not considered during planning, which are most of the systems in operation today.

#### 3.2.3 Contingency Analysis

To ensure the system is able to sustain its reliability under the proposed model for reducing Market Power cost, contingency analysis is considered in formulation (2.14). To represent the connection status of each transmission line during contingency, the parameter  $n_c$  (binary variable) is introduced in the formulation. The variable tests each line as a contingency element and evaluate its effects on



Figure 3.4: Marginal Cost Curve of  $u_3$ .

the system reliability including Optimal Transmission Switching to reduce market power cost.

When contingency is defined for a transmission lined, a new network topology is set. For this topology the program suggests an optimal planning for switching several lines in order to minimize the social cost. The proposed model considering contingency analysis is applied to the 14-node example system.

Contingency for each line is studied and results are presented in table 3.11. For most of the contingency cases transmission lines are optimally switched off to minimize the social cost, for these contingency cases the system remains stable. During the contingency analysis the Social Cost variate for different cases, some of them present an increase up to 9% of the social cost (for contingencies in line 2, line 3 and line 5 respectively) compared to the social cost for optimal transmission



Figure 3.5: Marginal Cost Curve of  $u_6$ .

switching under Nash Equilibria when there is no contingency (\$17764 MWh).

Observing table 3.11 the optimal transmission lines switched to reduce SC under contingency for the feasible results are mainly the same as the ones proposed in section 3.2.2. Then for these contingency scenarios it can be concluded that the system can sustain its reliability under the proposed model for reducing social cost.

Nevertheless this conclusions can not be generalized for all scenarios, table 3.11 shows infeasible results for several contingency conditions (35% of the contingency cases are infeasible). An infeasible solution stands for: there is no solution that fulfills all the constrains, the problem has no solution [5]. These infeasibilities do not necessarily reflect the stability of the system. There are two main reasons to which these infeasibility results can be attributed: (1) There is no Nash Equilibrium found in the system, there is no strategy that can be arranged between the



Figure 3.6: Marginal Cost Curve of  $u_5$ .

players (producers). (2) The mathematical model implemented is too simple to reach the solution.

Therefore taking into account all these considerations, the proposed model (optimal transmission switching to reduce market power cost) presents promising results to sustain the reliability of the system after a fault has occur.

Contingency	Open lines	SC [\$/MWh]
$L_1$	$L_8, L_{14}, L_{15}, L_{20}$	17964
$L_2$	$L_{1}, L_{14}$	19364
$L_3$	$L_8, L_{14}, L_{15}, L_{20}$	19364
$L_4$	-	infeasible
$L_5$	$L_{14}, L_{20}$	19364
$L_6$	-	infeasible
$L_7$	-	infeasible
$L_8$	$L_{14}, L_{15}, L_{20}$	17764
$L_9$	$L_{14}, L_{20}$	17764
$L_{10}$	$L_8, L_{12}, L_{14}, L_{15}, L_{20}$	18756
$L_{11}$	-	infeasible
$L_{12}$	$L_8, L_{14}, L_{15}, L_{20}$	17764
$L_{13}$	$L_8, L_{14}, L_{15}$	17764
$L_{14}$	$L_8, L_{15}, L_{20}$	17764
$L_{15}$	$L_8, L_{14}, L_{20}$	17764
$L_{16}$	-	infeasible
$L_{17}$	_	infeasible
L <sub>18</sub>	-	infeasible
$L_{19}$	$L_8, L_{14}, L_{15}, L_{20}$	17764
$L_{20}$	$L_8, L_{14}, L_{15}$	17764

Table 3.11: Contingency analysis ( SC & OTS under NE)

## Chapter 4

## **Conclusions and Future Work**

### 4.1 Conclusion

Nowadays deregulated markets face the problem that their transmission systems had been designed with mainly efficiency considerations, this affects the competitively of players, giving room for producer to exercise horizontal market power.

A mathematical model was developed to quantify the generation cost and reduce market power. Horizontal market power was reduced by restraining producers from withholding their generation capacity.

Optimal transmission switching is proposed with a Worst-Nash Equilibrium (maximizes Social Cost) linear optimization and tested on a 14-node example system.

The proposed mathematical formulation is based on game theory concepts (Nash equilibrium); the formulation includes strategic generators that might choose to withhold some of their output and non-strategic generators that offer their maximum production capacity to the market.

The proposed method has improved competition, reducing the total withheld capacity of the system from 70.4% to 55.8% of the installed capacity in strategic

generators. The system increases 51,43MW of generation capacity offer to the market. Results demonstrate that the Social Cost of the system has reduced up to 70.45%, increasing the efficiency of the market.

Including optimal transmission switching increases the economic benefit in systems designed with only reliability and efficiency planning considerations. This thesis gives a glance of the impact and how important it is for society that transmissions planning considers not only meeting the demand but also reducing the cost for society.

#### 4.2 Future Work

The proposed model considers a transmission switching formulation based on a DC Optimal Power Flow. Further studies consider the use of an AC Optimal Power Flow formulation to measure the impact of the transmission switching in the voltage levels, reactive power and transient stability.

A multi-period model is recommended to investigate the variations that are observed in the demand during the different seasons in a year and their impact in reducing market power.

Introducing optimal transmission switching in large scale can present a challenge due to large computational time. To make this feasible, the impact of optimal transmission switching in specific areas of the system should be studied closely to determine if they can affect the overall efficiency of the network.

A more detailed and stronger reliability criteria analysis must be carried and ensure reliability of the system after transmission switching. One consideration is that the example system was not congested before optimal transmission switching implementation; congested network previous switching must be taken into account to see how transmission switching (to regulate market power) can jeopardize the system reliability.

Future work includes optimal control of power flow capacity through the transmission lines to minimize market power cost by using power electronics in the transmission lines.

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GAMS Code

#### C:\Users\Maria\Desktop\appendix gams\14\_1.gms 25 September 2012 18:29:09

```
Page 1
```

```
1 * Modelling Optimal Transmission switching and Extremal Nash Equilibria in Wh»
  olesale Electricity Markets
 2 * Using a Single Stage Mixed Integer Linear Program
 3 *
 4 * This version: 1.0 (29 July 2012)
 5
 6
   Sets
 7
     p portfolios owning strategic generating units
 8
         /p1*p3/
9
     n set of connection nodes in the system
10
        /n1*n14/
11
    u generating units
12
        /u1*u11/
13
     owns(p,u) ownership relation between portfolios and units
14
        /p1.u3, p2.u6, p3.u7/
15
     nd(n,u) connection node of each generating unit
        /n1.ul, n2.u2, n3.u3, n3.u4, n8.u5, n13.u6, n6.u7, n3.u8, n14.u9, n4.ul»
16
  0, n9.u11/
17
    l transmission links
18
         /11*120/
     nt(n,l) conection node of each line
19
      /n1.l1, n2.l1, n1.l2, n5.l2, n2.l3, n3.l3, n2.l4, n4.l4, n2.l5, n5.l5, n»
20
   3.16, n4.16, n4.17, n5.17, n4.18, n7.18, n4.19, n9.19, n5.110, n6.110, n6.111»
   , n11.111,
        n6.112, n12.112, n6.113, n13.113, n7.114, n8.114, n7.115, n9.115, n9.11»
21
   6, n10.116, n9.117, n14.117, n10.118, n11.118, n12.119, n13.119, n13.120, n14»
   .120 /
22
     ss range of scenarios to be considered in a year /ss1/
23 ;
24 Parameters
25
    cost(u) variable cost of generating unit u dollars per MWh
         /u1 30, u2 20, u3 100, u4 10000, u5 5000, u6 100, u7 150, u8 100/
2.6
27
      cap(u,ss) maximum production capacity for unit u in MW
2.8
          /ul.ss1 30, u2.ss1 200, u3.ss1 150, u4.ss1 100, u5.ss1 100, u6.ss1 10»
29
   0, u7.ss1 100, u8.ss1 100/
30
31
    F(l,ss) flow limits
          /11.ss1 20, 12.ss1 20, 13.ss1 20, 14.ss1 20, 15.ss1 20, 16.ss1 20, 17»
32
   .ss1 20, 18.ss1 20, 19.ss1 20, 110.ss1 20, 111.ss1 20, 112.ss1 20, 113.ss1 20»
   , 114.ss1 20, 115.ss1 20, 116.ss1 20, 117.ss1 20, 118.ss1 20, 119.ss1 20, 120»
   .ss1 20/
33
34
     Fc(l,ss) flow limits
          /l1.ss1 20, l2.ss1 20, l3.ss1 20, l4.ss1 20, l5.ss1 20, l6.ss1 20, l7»
35
   .ss1 20, 18.ss1 20, 19.ss1 20, 110.ss1 20, 111.ss1 20, 112.ss1 20, 113.ss1 20»
   , 114.ss1 20, 115.ss1 20, 116.ss1 20, 117.ss1 20, 118.ss1 20, 119.ss1 20, 120»
   .ss1 20/
36
37
      C(l,n) incidence matrix
          /l1.n1 -1, l1.n2
                                1,
38
39
          12.n1
                  -1,
                       12.n5
                                1,
40
          13.n2
                  -1, 13.n3
                                1,
41
          14.n2
                 -1, 14.n4
                                1,
42
          15.n2
                 -1, 15.n5
                                1,
43
          16.n3
                  -1, 16.n4
                                1,
          17.n5
                  -1, 17.n4
44
                                1,
                       18.n7
45
          18.n4
                  -1,
                                1,
46
          19.n4
                  -1,
                       19.n9
                                1,
47
          l10.n5 -1, l10.n6 1,
48
          lll.n6 -1, lll.n9 1,
```

49 l12.n6 -1, l12.n12 1, 50 113.n6 -1, 113.n13 1, 51 l14.n7 -1, l14.n8 1, 52 l15.n7 -1, l15.n9 1, 53 l16.n9 -1, l16.n10 1, 54 l17.n9 -1, l17.n14 1, 55 118.n11 -1, 118.n10 1, l19.n12 -1, l19.n13 1, 56 57 120.n14 -1, 120.n13 1/ 58 59 CG(u,n) matrix of each generating unit connection's to node 60 /ul.nl 1, u2.n2 1, u3.n3 1, u4.n3 1, u5.n8 1, u6.n13 1, 61 u7.n6 1, u8.n3 1, u9.n14 1, u10.n4 1, u11.n9 1/ 62 63 D(n,ss) total demand 64 /n2.ss1 21.7, n3.ss1 94.2, n4.ss1 47.8, n5.ss1 7.6, n6.ss1 11.2, n9.ss» 1 29.5, n10.ss1 9, n11.ss1 3.5, n12.ss1 6.1, n13.ss1 13.5, n14.ss1 14.9/ 65 66 XX(1,ss) electrical reactance of line 1 67 /ll.ss1 0.05917, l2.ss1 0.22304, l3.ss1 0.19797, l4.ss1 0.17632, l5.ss» 1 0.17388, 16.ss1 0.17103, 17.ss1 0.04211, 18.ss1 0.20912, 19.ss1 0.55618, 11» 0.ss1 0.25202, 111.ss1 0.19890, 112.ss1 0.25581, 113.ss1 0.13027, 114.ss1 0.1» 7615, 115.ss1 0.11001, 116.ss1 0.08450, 117.ss1 0.27038, 118.ss1 0.19207, 119» .ss1 0.19988, 120.ss1 0.34802/ 68 69 B(l,ss) electrical susceptance of line 1 70 71 cl(l,ss) cost of removing a line /l1.ss1 5, l2.ss1 5, l3.ss1 5, l4.ss1 5, l5.ss1 5, l6.ss1 5, l7.ss1 5,» 72 18.ss1 5, 19.ss1 5, 110.ss1 5, 111.ss1 5, 112.ss1 5, 113.ss1 5, 114.ss1 5, 1» 15.ss1 5, 116.ss1 5, 117.ss1 5, 118.ss1 5, 119.ss1 5, 120.ss1 5/ 73 74 nc(l,ss) operation status of a line during contingency 75 /l1.ss1 1, l2.ss1 1, l3.ss1 1, l4.ss1 1, l5.ss1 1, l6.ss1 1, l7.ss1 1,» 18.ss1 1, 19.ss1 1, 110.ss1 1, 111.ss1 1, 112.ss1 1, 113.ss1 1, 114.ss1 1, 1» 15.ss1 1, 116.ss1 1, 117.ss1 1, 118.ss1 1, 119.ss1 1, 120.ss1 1/ 76 77 prob(ss) probability of each scenario 78 /ss1 1.0/ 79 80 num\_units(p) number of units in portfolio p; 81 82 num\_units(p)=sum(u\$owns(p,u),1); 83 B(l,ss) = 1/XX(l,ss)84 ; 85 86 \* The following variables will need to be changed according to the 87 \* number of actions per unit 88 89 **Sets** a possible actions for each unit 'a' 90 91 /q1\*q4/ 92 s enumeration of strategies for each portfolio n^a /s1\*s4/ 93 k index of binary digits - b1 LSB - log2(a) - /w1\*w4/ 94 95 \* For each portfolio the full list of potential strategies must be 96 \* listed. Each strategy must specify one and only one action for each 97 \* strategic unit 98 99 sl(p,s,u,a) list of allowed strategies for each portfolio 100 ps(p,s) list of strategies defined for each portfolio

```
101
      us(u) list of strategic generators
102
      un(u) list of non-strategic generators;
103
104 * Use this equation when portfolio p has only 1 unit
105
      sl(p,s,u,a)$(num_units(p)=1) = yes$(ord(s)=ord(a))*owns(p,u) ;
106
107 * The following equation only works when portfolio p has exactly 2 units
      sl(p, s, u, a) $ (num_units(p)=2)
108
109
               = yes$((mod(ord(s)-1,4)=(ord(a)-1))*owns(p,u)*(mod(ord(u),2)=1)) +
110
                 yes$((mod(trunc((ord(s)-1)/4),4)=(ord(a)-1))*owns(p,u)*(mod(ord(»))
   u),2)=0)) ;
111
112
      ps(p,s) = yes$(sum((u,a),sl(p,s,u,a)));
      us(u) = yes$(sum(p,owns(p,u)));
113
114
      un(u) = yes$(not us(u));
115
      alias(p,cp) ;
116
     alias(s,cs) ;
117
118
119 Parameters
     BigM a big number /999999/
120
121
      w0 additive offset for constant
122
      w(k) conversion factor from binary to production
123
     y(a,k) mapping from unit action to share of output ;
124
125
     y(a,k) = mod(trunc((ord(a)-1)/power(2, ord(k)-1)), 2);
126
127
     w0 = power(2,-card(k));
128
      w(k) = power(2, -(card(k) - ord(k) + 1));
129
130
131 Table CT(n, 1) transpose of the incidence matrix 'all data are logged and in »
    csv format'
132 11 12 13 14 15 16 17 18 19 110 111 112 113 114 115 116 117 118 119 120
133
134 $ondelim
135 $include matrices_14.csv
136 $offdelim
137
138 Variables
139
     social_cost
140
     F10(1,ss)
     Fl0c(l,ss)
141
142
      theta0(n,ss)
      theta0c(n,ss)
143
144
     Fl(cp,cs,l,ss)
145
     Flc(cp,cs,l,ss)
146
     theta(cp,cs,n,ss)
147
     thetac(cp,cs,n,ss)
148
      pi0(p,ss) profit of portfolio p
     pi(cp,cs,p,ss) profit of portfolio p in case (cp cs)
149
150
      ;
151 Free variable
152
    rho0(n,ss)
153
     delta0(n,ss)
154
     rho(cp,cs,n,ss)
155
      delta(cp,cs,n,ss)
156
157 Positive Variables
158
     q0(u,ss)
159
      gh0(u,ss)
```

160

219

z0(u,k,ss)

```
161
     g(cp,cs,u,ss)
162
     gh(cp,cs,u,ss)
163
     z(cp,cs,u,k,ss)
164
165
     lambdadown0(1,ss)
     mudown0(u,ss)
166
     betadown0(l,ss)
167
     alphadown0(l,ss)
168
169
     epsilondown0(l,ss)
170
    lambdaup0(l,ss)
171 muup0(u,ss)
172
     betaup0(1,ss)
173
     alphaup0(1,ss)
174
      epsilonup0(l,ss)
175
      lambdadown(cp,cs,l,ss)
176
     mudown(cp,cs,u,ss)
177
     betadown(cp,cs,l,ss)
178
     alphadown(cp,cs,l,ss)
179
     epsilondown(cp,cs,l,ss)
180
     lambdaup(cp,cs,l,ss)
     muup(cp,cs,u,ss)
181
182
     betaup(cp,cs,l,ss)
183
     alphaup(cp,cs,l,ss)
184
      epsilonup(cp,cs,l,ss)
185
      ;
186 Binary Variables
187
     nl(l,ss)
188
      x0(u,k,ss)
189
      x(cp,cs,u,k,ss)
190
     b_lambdadown0(l,ss)
191
     b_mudown0(u,ss)
192
     b_betadown0(1,ss)
193
     b_alphadown0(l,ss)
194
     b_epsilondown0(l,ss)
195
     b_lambdaup0(l,ss)
196
      b_muup0(u,ss)
197
     b_betaup0(1,ss)
198
     b_alphaup0(l,ss)
199
     b_epsilonup0(1,ss)
200
     b_lambdadown(cp,cs,l,ss)
201
     b_mudown(cp,cs,u,ss)
202
     b_betadown(cp,cs,l,ss)
203
      b_alphadown(cp,cs,l,ss)
204
     b_epsilondown(cp,cs,l,ss)
205
     b_lambdaup(cp,cs,l,ss)
206
     b_muup(cp,cs,u,ss)
207
     b_betaup(cp,cs,l,ss)
208
      b_alphaup(cp,cs,l,ss)
209
      b_epsilonup(cp,cs,l,ss)
210
      ;
211
212 *Objective function - social cost
213
214 Equations
215
      obj
216 ;
217
218 obj ..
                        social_cost =e= (sum{ss,prob(ss)*sum(u,cost(u)*q0(u,ss))»
    }+sum{(l,ss),cl(l,ss)*(1-nl(l,ss))}) ;
```

;

```
221 *Optimal dispatch for the candidate WNE
223
224 Equations
225
226
    e01_0(u,ss) volume of capacity that its offer to the market
    e02_0(p,ss) profit of a portafolio
227
228
    eA_0(u,k,ss) linearization of equation gh0
    eB_0(u,k,ss) linearization of equation gh0
229
230
     eC_0(u,k,ss) linearization of equation gh0
      eD_0(u,k,ss) linearization of equation gh0
231
232 ;
                    gh0(u,ss) =e= (w0 + sum(k,w(k)*x0(u,k,ss)))*cap(u,ss);
233 e01_0(u,ss) ..
234 e02_0(p,ss) ..
                      pi0(p,ss) =e= sum(u$owns(p,u),(muup0(u,ss)*w0 + sum(k,w»
   (k) * z0(u, k, ss))) * cap(u, ss));
235 eA_0(us,k,ss) .. z0(us,k,ss)-muup0(us,ss) =l= BigM*(1-x0(us,k,ss));
236 eB_0(us,k,ss) ..
                     z0(us,k,ss)-muup0(us,ss) =g= -BigM*(1-x0(us,k,ss));
237 eC_0(us,k,ss) .. z0(us,k,ss) =l= BigM*x0(us,k,ss);
238 eD_0(u,k,ss)$un(u) .. x0(u,k,ss) =e= 1;
239
240 * KKT conditions
241 * Primal
242 *
      DCOPF problem with optimal transmission switching
243
244 Equations
245
246
     e2_0(u,ss) maximun generation
247
    e5_0(1,ss) maximun power flow across line limit
248
    e6_0(1,ss) minimun power flow across line limit
249
    e7_0(n,ss) power balance at each node
250
    e8_0(1,ss) kirchhoff's laws
251
     e9_0(l,ss) kirchhoff's laws
252
253 ;
254 e2_0(u,ss) ..
                     g0(u,ss)=l= gh0(u,ss);
255 e5_0(l,ss) ..
                     Fl0(l,ss) =l= F(l,ss)*nl(l,ss);
256 e6_0(l,ss) ..
                     Fl0(l,ss) =g= -F(l,ss)*nl(l,ss);
                     sum(1, F10(1,ss)*C(1,n))+(sum(u$nd(n,u),g0(u,ss))-D(n,s»
257 e7_0(n,ss) ..
   s))=e=0;
258 e8_0(l,ss) ..
                      sum{n, B(l,ss)*C(l,n)*theta0(n,ss)}- Fl0(l,ss)+(1-nl(l,»
   ss))*BigM =g= 0;
259 e9_0(l,ss) ..
                      sum{n, B(l,ss)*C(l,n)*theta0(n,ss)}- Fl0(l,ss)-(1-nl(l,»
   ss))*BigM =l= 0;
260
261 *
      DCOPF optimal transmission switching with contingency analysis
262
263 Equations
264
      e12_0(1,ss) maximun power flow across line limit for contingency c
265
266
      e13_0(1,ss) minimun power flow across line limit for contingency c
267
      e14_0(n,ss) power balance at each node for contingency c
268
      e15_0(l,ss) kirchhoff's laws for contingency c
      e16_0(l,ss) kirchhoff's laws for contingency c
269
270 ;
271 e12_0(l,ss) ..
                      FlOc(l,ss) =l= Fc(l,ss)*nl(l,ss)*nc(l,ss);
272 e13_0(l,ss) ..
                      FlOc(l,ss) =g= -Fc(l,ss)*nl(l,ss)*nc(l,ss);
273 e14_0(n,ss) ..
                     sum(1, Fl0c(1,ss)*C(1,n))+(sum(u$nd(n,u),g0(u,ss))-D(n,»
   ss))=e=0;
```
Page 6

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274 e15_0(l,ss) ..
                          sum{n, B(1,ss)*C(1,n)*theta0c(n,ss)}- Fl0c(1,ss)+(2-n1(»)
    l,ss)-nc(l,ss))*BigM =g= 0;
275 e16_0(l,ss) ..
                          sum{n, B(l,ss)*C(l,n)*theta0c(n,ss)}- Fl0c(l,ss)-(2-nl(»
    l,ss)-nc(l,ss))*BigM =l= 0;
276
277 * Stationary conditions
278
279 Equations
280
281
       e17_0(u,ss) derivate of Lagrangian respect to the generation of each unit
282
       e18_0(n,ss) derivate of Lagrangian respect to the voltage angle of each no»
   de
283
       e19_0(1,ss) derivate of Lagrangian respect to the power flow of each line
       e20_0(n,ss) derivate of Lagrangian respect to the voltage angle of each no»
284
   de during contingency c
285
       e21_0(l,ss) derivate of Lagrangian respect to the power flow of each line »
   during contingency c
286 ;
287 e17_0(u,ss) ..
                          -\cot(u) + \mathbf{sum}(n, rho0(n, ss) * CG(u, n)) - mudown0(u, ss) + muup0 >>
    (u,ss)+sum(n, delta0(n,ss)*CG(u,n))=e=0;
288 e18_0(n,ss) ..
                          sum{1, CT(n,1)*betadown0(1,ss)*B(1,ss)}-sum{1, CT(n,1)*>
    betaup0(1,ss)*B(1,ss) ===0;
289 e19_0(l,ss) ..
                          sum(n, rho0(n,ss)*C(l,n))-lambdadown0(l,ss)+lambdaup0(l»
    ,ss)+betadown0(l,ss)-betaup0(l,ss)=e=0;
290 e20_0(n,ss) ..
                          sum{l, CT(n,l)*epsilondown0(l,ss)*B(l,ss)}-sum{l, CT(n,»
    l) *epsilonup0(l, ss) *B(l, ss) }=e=0;
291 e21_0(l,ss) ..
                          sum(n, delta0(n,ss)*C(l,n))-alphadown0(l,ss)+alphaup0(l»
    ,ss)+epsilondown0(l,ss)-epsilonup0(l,ss)=e=0;
292
293 * Complementary slackness conditions
294 * Reformulating as a Mix Integer Linear Programming Problem (MILP)
295
296 Equations
297
298
       e36_0(1,ss) Lower boundary of the capacity constraints on transmission lin»
    es as MILP
299
       e37_0(1,ss) Lower boundary of the capacity constraints on transmission lin»
    es as MILP
300
     e38_0(1,ss) Lower boundary of the capacity constraints on transmission lin»
    es as MILP
301
     e39_0(1,ss) Lower boundary of the capacity constraints on transmission lin»
    es as MILP
302
      e40_0(l,ss) Upper boundary of the capacity constraints on transmission lin»
   es as MILP
303
      e41_0(l,ss) Upper boundary of the capacity constraints on transmission lin»
   es as MILP
304
     e42_0(1,ss) Upper boundary of the capacity constraints on transmission lin»
    es as MILP
305
     e43_0(1,ss) Upper boundary of the capacity constraints on transmission lin»
    es as MILP
306
       e44_0(u,ss) Lower boundary of the capacity constraints on each generating »
   units as MILP
       e45_0(u,ss) Lower boundary of the capacity constraints on each generating »
307
    units as MILP
308
       e46_0(u,ss) Lower boundary of the capacity constraints on each generating »
   units as MILP
309
       e47_0(u,ss) Lower boundary of the capacity constraints on each generating »
   units as MILP
      e48_0(u,ss) Upper boundary of the capacity constraints on each generating »
310
   units as MILP
       e49_0(u,ss) Upper boundary of the capacity constraints on each generating »
311
```

units as MILP 312 e50\_0(u,ss) Upper boundary of the capacity constraints on each generating » units as MILP 313 e51\_0(u,ss) Upper boundary of the capacity constraints on each generating » units as MILP 314 e52\_0(1,ss) Lower boundary of constraints on kirchhoff's laws as MILP e53\_0(l,ss) Lower boundary of constraints on kirchhoff's laws as MILP 315 316 e54\_0(l,ss) Lower boundary of constraints on kirchhoff's laws as MILP 317 e55\_0(l,ss) Lower boundary of constraints on kirchhoff's laws as MILP 318 e56\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP 319 e57\_0(l,ss) Upper boundary of constraints on kirchhoff's laws as MILP 320 e58\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP 321 e59\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP e68\_0(1,ss) Lower boundary of the capacity constraints on transmission lin» 322 es as MILP for contingency c 323 e69\_0(1,ss) Lower boundary of the capacity constraints on transmission lin» es as MILP for contingency c 324 e70\_0(1,ss) Lower boundary of the capacity constraints on transmission lin» es as MILP for contingency c 325 e71\_0(1,ss) Lower boundary of the capacity constraints on transmission lin» es as MILP for contingency c e72\_0(l,ss) Upper boundary of the capacity constraints on transmission lin» 326 es as MILP for contingency c 327 e73\_0(1,ss) Upper boundary of the capacity constraints on transmission lin» es as MILP for contingency c 328 e74\_0(1,ss) Upper boundary of the capacity constraints on transmission lin» es as MILP for contingency c e75\_0(1,ss) Upper boundary of the capacity constraints on transmission lin» 329 es as MILP for contingency c 330 e76\_0(l,ss) Lower boundary of constraints on kirchhoff's laws as MILP for » contingency c 331 e77\_0(l,ss) Lower boundary of constraints on kirchhoff's laws as MILP for » contingency c 332 e78\_0(1,ss) Lower boundary of constraints on kirchhoff's laws as MILP for » contingency c 333 e79\_0(1,ss) Lower boundary of constraints on kirchhoff's laws as MILP for » contingency c 334 e80\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP for » contingency c 335 e81\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP for » contingency c 336 e82\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP for » contingency c 337 e83\_0(1,ss) Upper boundary of constraints on kirchhoff's laws as MILP for » contingency c 338 ; 339 340 e36\_0(l,ss) .. -biqM\*(1-b\_lambdadown0(l,ss))=l= (-F(l,ss)\*nl(l,ss)-F10» (1,ss)); 341 e37\_0(l,ss) .. (-F(l,ss)\*nl(l,ss)-Fl0(l,ss))=l= bigM\*(1-b\_lambdadown0(» 1,ss)); 342 e38\_0(l,ss) .. -bigM\*(b\_lambdadown0(l,ss))=l=lambdadown0(l,ss); lambdadown0(l,ss)=l=bigM\*(b\_lambdadown0(l,ss)); 343 e39\_0(l,ss) .. 344 e40\_0(l,ss) .. -bigM\*(1-b\_lambdaup0(l,ss))=1=(F10(l,ss)-F(l,ss)\*nl(l,s» s));

345 e41\_0(l,ss) .. (Fl0(l,ss)-F(l,ss)\*nl(l,ss))=l= bigM\*(1-b\_lambdaup0(l,s»

 346 e42\_0(l,ss) ..
 -bigM\*(b\_lambdaup0(l,ss))=l=lambdaup0(l,ss);

 347 e43\_0(l,ss) ..
 lambdaup0(l,ss)=l=bigM\*(b\_lambdaup0(l,ss));

349 e44\_0(u,ss) .. -bigM\*(1-b\_mudown0(u,ss))=l= (-g0(u,ss));

s));

348

```
350 e45_0(u,ss) ..
                       (-q0(u, ss)) = l = biqM^{(1-b_mudown0(u, ss))};
351 e46_0(u,ss) ..
                       -bigM*(b_mudown0(u,ss))=l=mudown0(u,ss);
352 e47_0(u,ss) ..
                       mudown0(u,ss)=l= bigM*(b_mudown0(u,ss));
353 e48_0(u,ss) ..
                       -bigM*(1-b_muup0(u,ss))=l=(g0(u,ss)-gh0(u,ss));
354 e49_0(u,ss) ..
                       (g0(u,ss)-gh0(u,ss))=l= bigM*(1-b_muup0(u,ss));
355 e50_0(u,ss) ..
                       -bigM*(b_muup0(u,ss))=l=muup0(u,ss);
356 e51_0(u,ss) ..
                       muup0(u,ss)=l=bigM*(b_muup0(u,ss));
357
358 e52_0(l,ss) ..
                       -bigM*(1-b_betadown0(l,ss))=1= sum{n, (-B(l,ss))*C(l,n)*»
   theta0(n,ss)}+ Fl0(l,ss)-(1-nl(l,ss))*BigM;
359 e53_0(l,ss) ..
                       sum{n, (-B(l,ss))*C(l,n)*theta0(n,ss)}+ Fl0(l,ss)-(1-nl(»
   l,ss))*BigM =l= bigM*(1-b_betadown0(l,ss));
360 e54_0(l,ss) ..
                       -bigM*(b_betadown0(l,ss))=l=betadown0(l,ss);
361 e55_0(l,ss) ..
                      betadown0(l,ss)=l=bigM*(b_betadown0(l,ss));
362 e56_0(l,ss) ..
                       -bigM*(1-b_betaup0(l,ss))=l= sum{n,B(l,ss)*C(l,n)*theta»
   0(n,ss) - Fl0(l,ss) - (1-nl(l,ss)) *BiqM;
363 e57_0(l,ss) ..
                       sum{n,B(l,ss)*C(l,n)*theta0(n,ss)}- Fl0(l,ss)-(1-nl(l,s»
   s))*BiqM =l= biqM*(1-b_betaup0(l,ss));
                       -bigM*(b_betaup0(1,ss)) = 1 = betaup0(1,ss);
364 e58_0(l,ss) ..
365 e59_0(l,ss) ..
                       betaup0(l,ss)=l=bigM*(b_betaup0(l,ss));
366
367 e68_0(l,ss) ..
                       -bigM*(1-b_alphadown0(1,ss))=1= (-Fc(1,ss)*nl(1,ss)*nc(»
   l,ss)-FlOc(l,ss));
368 e69_0(l,ss) ..
                       (-Fc(l,ss)*nl(l,ss)*nc(l,ss)-FlOc(l,ss))=l= bigM*(1-b_a»
   lphadown0(l,ss));
369 e70_0(l,ss) ..
                       -bigM*(b_alphadown0(l,ss))=l=alphadown0(l,ss);
370 e71_0(l,ss) ..
                       alphadown0(l,ss)=l=bigM*(b_alphadown0(l,ss));
371 e72_0(l,ss) ..
                       -bigM*(1-b_alphaup0(1,ss))=l=(Fl0c(1,ss)-Fc(1,ss)*nl(1,»
   ss)*nc(l,ss));
372 e73_0(l,ss) ..
                       (FlOc(l,ss)-Fc(l,ss)*nl(l,ss)*nc(l,ss))=l= bigM*(1-b_al»
   phaup0(l,ss));
373 e74_0(l,ss) ..
                       -bigM*(b_alphaup0(l,ss))=l=alphaup0(l,ss);
374 e75_0(l,ss) ..
                       alphaup0(l,ss)=l=bigM*(b_alphaup0(l,ss));
375
376 e76_0(l,ss) ..
                       -bigM*(1-b_epsilondown0(l,ss))=1= sum{n,(-B(l,ss))*C(l,»
   n)*theta0c(n,ss)}+ Fl0c(l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM;
377 e77_0(l,ss) ..
                       sum{n, (-B(1,ss))*C(1,n)*theta0c(n,ss)}+ Fl0c(1,ss)-(2-n»
   l(l,ss)-nc(l,ss))*BiqM =l= biqM*(1-b_epsilondown0(l,ss));
378 e78_0(l,ss) .. -bigM*(b_epsilondown0(l,ss))=l=epsilondown0(l,ss);
379 e79_0(l,ss) ..
                      epsilondown0(l,ss)=l=bigM*(b_epsilondown0(l,ss));
                       -biqM*(1-b_epsilonup0(1,ss))=1= sum{n,B(1,ss)*C(1,n)*th»
380 e80_0(l,ss) ..
   eta0c(n,ss)}- Fl0c(l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM;
381 e81_0(l,ss) ..
                      sum{n,B(l,ss)*C(l,n)*theta0c(n,ss)}- Fl0c(l,ss)-(2-nl(l)*
   ,ss)-nc(l,ss))*BigM =l= bigM*(1-b_epsilonup0(l,ss));
382 e82_0(l,ss) ..
                      -bigM*(b_epsilonup0(l,ss))=l=epsilonup0(l,ss);
383 e83_0(l,ss) ..
                       epsilonup0(l,ss)=l= bigM*(b_epsilonup0(l,ss));
384
386 *Optimal dispatch for the alternative case p s
388
389 Equations
390
391
      e01(cp,cs,u,ss) volume of capacity that its offer to the market
392
      e02(cp,cs,p,ss) profit of a portafolio
      eA(cp,cs,u,k,ss) linearization of equation gh0
393
394
      eB(cp,cs,u,k,ss) linearization of equation gh0
395
      eC(cp,cs,u,k,ss) linearization of equation gh0
396
      eD(cp,cs,u,k,ss) linearization of equation gh0
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397 ;
398 e01(cp,cs,u,ss)
                            gh(cp,cs,u,ss) =e= (w0 + sum(k,w(k)*x(cp,cs,u,k,ss)»
                    ••
   ))*cap(u,ss);
399 e02(cp,cs,p,ss) ..
                            pi(cp,cs,p,ss) =e= sum(u$owns(p,u),(muup(cp,cs,u,ss»
   )*w0 + sum(k,w(k)*z(cp,cs,u,k,ss)))*cap(u,ss));
400 eA(cp,cs,us,k,ss) .. z(cp,cs,us,k,ss)-muup(cp,cs,us,ss) =l= BigM*(1-x(cp»
    ,cs,us,k,ss));
401 eB(cp,cs,us,k,ss) .. z(cp,cs,us,k,ss) =l= BigM*x(cp,cs,us,k,ss);
402 eC(cp,cs,us,k,ss) ..
                            z(cp,cs,us,k,ss)-muup(cp,cs,us,ss) =g= -BigM*(1-x(c»
   p,cs,us,k,ss));
403 eD(cp,cs,u,k,ss)
                            x(cp,cs,u,k,ss) =e= x0(u,k,ss)$(not owns(cp,u)) + s»
                    ..
   um(a,y(a,k)$sl(cp,cs,u,a))$owns(cp,u);
404
405 * KKT conditions
406 * Primal
407 *
       DCOPF problem with optimal transmission switching
408
409 Equations
410
     e2(cp,cs,u,ss) maximun generation
411
     e5(cp,cs,l,ss) maximun power flow across line limit
412
      e6(cp,cs,l,ss) minimun power flow across line limit
413
414
     e7(cp,cs,n,ss) power balance at each node
415
     e8(cp,cs,l,ss) kirchhoff's laws
416
     e9(cp,cs,l,ss) kirchhoff's laws
417 ;
418 e2(cp,cs,u,ss) ..
                             q(cp, cs, u, ss) = l = qh(cp, cs, u, ss);
                            Fl(cp,cs,l,ss) =l= F(l,ss)*nl(l,ss);
419 e5(cp,cs,l,ss) ..
                            Fl(cp,cs,l,ss) =g= -F(l,ss)*nl(l,ss);
420 e6(cp,cs,l,ss) ..
421 e7(cp,cs,n,ss) ...
                             sum(1, F1(cp,cs,l,ss)*C(l,n))+(sum(u$nd(n,u),g(cp,c»
   s,u,ss))-D(n,ss))=e=0;
422 e8(cp,cs,l,ss) ..
                             sum{n, B(l,ss)*C(l,n)*theta(cp,cs,n,ss)}- Fl(cp,cs,»
   l,ss)+(1-nl(l,ss))*BigM =g= 0;
423 e9(cp,cs,l,ss) ..
                            sum{n, B(l,ss)*C(l,n)*theta(cp,cs,n,ss)}- Fl(cp,cs,»
   l,ss)-(1-nl(l,ss))*BigM =l= 0;
424
425 *
        DCOPF optimal transmission switching with contingency analysis
426
427 Equations
428
429
      e12(cp,cs,l,ss) maximun power flow across line limit for contingency c
430
      e13(cp,cs,l,ss) minimun power flow across line limit for contingency c
431
      el4(cp,cs,n,ss) power balance at each node for contingency c
432
      e15(cp,cs,l,ss) kirchhoff's laws for contingency c
433
      el6(cp,cs,l,ss) kirchhoff's laws for contingency c
434 ;
435 e12(cp,cs,l,ss) ...
                            Flc(cp,cs,l,ss) = l = Fc(l,ss)*nl(l,ss)*nc(l,ss);
436 e13(cp,cs,l,ss) ...
                            Flc(cp,cs,l,ss) = q = -Fc(l,ss)*nl(l,ss)*nc(l,ss);
437 e14(cp,cs,n,ss) ..
                             sum(1, Flc(cp,cs,l,ss)*C(1,n))+(sum(u$nd(n,u),g(cp,»
   cs,u,ss))-D(n,ss))=e=0;
438 e15(cp,cs,l,ss) ..
                             sum{n, B(l,ss)*C(l,n)*thetac(cp,cs,n,ss)}- Flc(cp,c»
   s,l,ss)+(2-nl(l,ss)-nc(l,ss))*BigM =g= 0;
                             sum{n, B(l,ss)*C(l,n)*thetac(cp,cs,n,ss)}- Flc(cp,c»
439 e16(cp,cs,l,ss) ..
   s,l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM =l= 0;
440
441 * Stationary conditions
442
443 Equations
444
445
      el7(cp,cs,u,ss) derivate of Lagrangian respect to the generation of each u»
   nit
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446
      e18(cp,cs,n,ss) derivate of Lagrangian respect to the voltage angle of eac»
   h node
447
      e19(cp,cs,l,ss) derivate of Lagrangian respect to the power flow of each l»
   ine
448
      e20(cp,cs,n,ss) derivate of Lagrangian respect to the voltage angle of eac»
   h node during contingency c
449
      e21(cp,cs,l,ss) derivate of Lagrangian respect to the power flow of each l»
    ine during contingency c
450 ;
451 e17(cp,cs,u,ss) ..
                             -cost(u)+sum(n, rho(cp,cs,n,ss)*CG(u,n))-mudown(cp,»
   cs,u,ss)+muup(cp,cs,u,ss)+sum(n, delta(cp,cs,n,ss)*CG(u,n))=e=0;
                            sum{1, CT(n,1)*betadown(cp,cs,1,ss)*B(1,ss)}-sum{1,»
452 e18(cp,cs,n,ss) ..
    CT(n, 1) *betaup(cp, cs, 1, ss) *B(1, ss)}=e=0;
                             sum(n, rho(cp,cs,n,ss)*C(l,n))-lambdadown(cp,cs,l,s»
453 e19(cp,cs,l,ss) ..
    s)+lambdaup(cp,cs,l,ss)+betadown(cp,cs,l,ss)-betaup(cp,cs,l,ss)=e=0;
454 e20(cp,cs,n,ss) ..
                            sum{1, CT(n,1)*epsilondown(cp,cs,1,ss)*B(1,ss)}-sum»
    {l, CT(n,l)*epsilonup(cp,cs,l,ss)*B(l,ss)}=e=0;
                             sum(n, delta(cp,cs,n,ss)*C(l,n))-alphadown(cp,cs,l,»
455 e21(cp,cs,l,ss) ..
   ss)+alphaup(cp,cs,l,ss)+epsilondown(cp,cs,l,ss)-epsilonup(cp,cs,l,ss)=e=0;
456
457 * Complementary slackness conditions
458 * Reformulating as a Mix Integer Linear Programming Problem (MILP)
459
460 Equations
461
462
      e36(cp,cs,l,ss) Lower boundary of the capacity constraints on transmission»
    lines as MILP
463
      e37(cp,cs,l,ss) Lower boundary of the capacity constraints on transmission»
    lines as MILP
464
      e38(cp,cs,l,ss) Lower boundary of the capacity constraints on transmission»
    lines as MILP
465
     e39(cp,cs,l,ss) Lower boundary of the capacity constraints on transmission»
    lines as MILP
466
     e40(cp,cs,l,ss) Upper boundary of the capacity constraints on transmission»
    lines as MILP
467
     e41(cp,cs,l,ss) Upper boundary of the capacity constraints on transmission»
     lines as MILP
468
     e42(cp,cs,l,ss) Upper boundary of the capacity constraints on transmission»
    lines as MILP
469
      e43(cp,cs,l,ss) Upper boundary of the capacity constraints on transmission»
    lines as MILP
470
      e44(cp,cs,u,ss) Lower boundary of the capacity constraints on each generat»
    ing units as MILP
471
      e45(cp,cs,u,ss) Lower boundary of the capacity constraints on each generat»
   ing units as MILP
472
     e46(cp,cs,u,ss) Lower boundary of the capacity constraints on each generat»
   ing units as MILP
473
     e47(cp,cs,u,ss) Lower boundary of the capacity constraints on each generat»
    ing units as MILP
474
      e48(cp,cs,u,ss) Upper boundary of the capacity constraints on each generat»
    ing units as MILP
475
      e49(cp,cs,u,ss) Upper boundary of the capacity constraints on each generat»
    ing units as MILP
476
      e50(cp,cs,u,ss) Upper boundary of the capacity constraints on each generat»
   ing units as MILP
477
      e51(cp,cs,u,ss) Upper boundary of the capacity constraints on each generat»
   ing units as MILP
478
      e52(cp,cs,l,ss) Lower boundary of constraints on kirchhoff's laws as MILP
479
      e53(cp,cs,l,ss) Lower boundary of constraints on kirchhoff's laws as MILP
480
      e54(cp,cs,l,ss) Lower boundary of constraints on kirchhoff's laws as MILP
      e55(cp,cs,l,ss) Lower boundary of constraints on kirchhoff's laws as MILP
481
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482	e56(cp,cs,l,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	
483	e57(cp,cs,l,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	
484	e58(cp,cs,l,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	
485	e59(cp,cs,l,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	
486	e68(cp,cs,l,ss)	Lower	boundary	of	the	capacit	у с	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngency c										
487	e69(cp,cs,l,ss)	Lower	boundary	of	the	capacit	у с	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngency c										
488	e70(cp,cs,l,ss)	Lower	boundary	of	the	capacit	у с	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngency c										
489	e71(cp,cs,l,ss)	Lower	boundary	of	the	capacit	y co	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngency c			1	-						
490	e72(cp,cs,l,ss)	Upper	boundary	of	the	capacit	V C	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngency c			1	1						
491	e73(cp,cs,l,ss)	Upper	boundarv	of	the	capacit	V C	onstraint	s or	n trar	ısmi	ssio	n»
	lines as MILP for	contir	ngencv c	-		1	1 -				-		
492	e74 (cp. cs. ]. ss)	Upper	boundary	of	the	capacit	V C	onstraint	s or	n trar	ısmi	ssio	n»
172	lines as MILP for	contir	gency c	ΟŦ	0110	capacito	y 0.	0110 01 01110	0 01	i crui	101111	0010	
493	$e^{75}(cp, cs, l, ss)$	Unner	boundary	of	the	capacit	VC	onstraint	s or	n trar	lsmi	ssio	n»
195	lines as MILP for	contir		01	CIIC	cupucit	y c.	onderarite	5 01	i crui	IOIIII	0010	
лал	$= \frac{1}{2} $	Lower	boundary	of	cone	etrainte	on	kirchhof	flo	1 2 10 0	25	мттр	
171	for contingency c	HOWEL	boundary	ΟL	COIL	scraincs	011	KIICIIIIOI	LS	Iaws	as		//
105	o <sup>77</sup> (ap as 1 as)	Lowor	houndary	of	aona	rtrainta	<u></u>	kirabbof	flo	1 2 10	20	MTTD	~~~~
495	for contingonau a	LOWEL	boundary	01	COIIS	straints	011	KIICIIIOI	LS	Laws	as	МІЦР	"
106	101 contingency c	Torrow	boundant	٥f		-+ wo i n+ o		l. i wabbaf	fla	1	~ ~	MTTD	
496	e/8(cp,cs,1,ss)	rowet.	boundary	OL	COUR	straints	OII	KILCUUOT	L·S	laws	as	MILP	<i>»</i>
407	for contingency c	Ŧ	, ,	c					c .	-		MITE	
497	e/9(cp,cs,1,ss)	Lower	boundary	OI	cons	straints	on	Kirchnor	I'S	laws	as	MILP	»
400	for contingency c		, ,	c					c .	-		MITE	
498	e80(cp,cs,1,ss)	Upper	boundary	OI	cons	straints	on	Kirchhoi	I'S	laws	as	MILP	»
	for contingency c			-					<i>.</i> .	-			
499	e81(cp,cs,1,ss)	Upper	boundary	oÍ	cons	straints	on	kirchhof	ʻs'	laws	as	MILP	»
	for contingency c			-					<i>.</i> .	-			
500	e82(cp,cs,1,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	»
	for contingency c												
501	e83(cp,cs,l,ss)	Upper	boundary	of	cons	straints	on	kirchhof	f's	laws	as	MILP	»
	for contingency c												
502	;												
503													
504	e36(cp,cs,l,ss)		-bigM*(1	l−b_	_lamb	odadown (	cp,	cs,l,ss))	=1=	(-F(]	.,ss	)*nl	( »
	l,ss)-Fl(cp,cs,l,ss	3)) <b>;</b>											
505	e37(cp,cs,l,ss)		(-F(l,s	s)*1	nl(l,	,ss)-Fl(	cp,	cs,l,ss))	=1=	bigM'	·(1-	b_la	m≫
	bdadown(cp,cs,l,ss)	));											
506	e38(cp,cs,l,ss)		-bigM*()	o_la	ambda	adown (cp	, CS	,l,ss))=1	=lan	nbdado	own (	cp,c	s»
	,l,ss);												
507	e39(cp,cs,l,ss)		lambdad	own	(cp,	cs,l,ss)	=1=]	bigM*(b_l	ambo	dadowr	ı(cp	,cs,	l»
	,ss));												
508	e40(cp,cs,l,ss)		-bigM*(2	L-b_	_lamb	odaup(cp	,cs	,l,ss))=1	=(F]	(cp,	:s,1	,ss)	-»
	F(l,ss)*nl(l,ss));												
509	e41(cp,cs,l,ss)		(Fl(cp,	cs,	l,ss)	)-F(1,ss	)*n	l(l,ss))=	l= k	bigM*	(1-t	_lam	b»
	<pre>daup(cp,cs,l,ss));</pre>		_							-			
510	e42(cp,cs,l,ss)		-biqM*()	5 la	ambda	aup(cp,c	s,l	,ss))=l=l	ambo	laup(c	cp,c	s,1,	s»
	s);					1 . 1 .				1 .	1,		
511	e43(cp,cs,l,ss)		lambdau	cr	o,cs,	,1,ss)=1	=bi	qM*(b lam	bdaı	ıp(cp,	cs,	l,ss	) »
	);		1	• 1						1 . 1 ,	,	,	
512	· •												
513	e44(cp,cs,u.ss)		-biaM*(	l-h	muda	own(cn.c	S.11	,ss))=]=	(-a	(cp.cs)	5,11-	ss))	;
514	e45(cp, cs, u, ss)		(-a(cp))	-~ יגאני	1, 55	) = l = hi	aM*	(1-b mudo	wn (a		.u.s	s)):	,
515	$e46(cp, cs_{11}, ss)$		-biaM*()	ר ב- היית כ	100wr	$(c_{D}, c_{S})$	11 - 91	s))=l=mud	Own	$(cp_{-}cs)$	~, 0 3. 11	ss).	
516	$e47(cp, cs_{11}, ss)$	mudown(cp, cs, u, ss) = l = higM*(h mudown(cp, cs, u, ss))											
517	e48(cp, cs, u, ss)		-biaM*(	- <b></b> h	m1111r	(cn.cs)	11.5	s))=]=(ơ(	cp - q	-r, 00, CS, 11. 9	-(ss		с»
~ ± /	$(0_{P}, 0_{P}, 0_{P},$		~rgm (.				a <b>,</b> 0,	-,, <u>-</u> (9)	-r,		,	3(0	~ ′′
	, , _ , , , , ,												

```
518 e49(cp,cs,u,ss) ..
                            (g(cp,cs,u,ss)-gh(cp,cs,u,ss))=l= bigM*(1-b_muup(cp»
    ,cs,u,ss));
519 e50(cp,cs,u,ss) ..
                            -bigM*(b_muup(cp,cs,u,ss))=l=muup(cp,cs,u,ss);
520 e51(cp,cs,u,ss) ..
                           muup(cp,cs,u,ss)=l=bigM*(b_muup(cp,cs,u,ss));
521
522 e52(cp,cs,l,ss) ..
                           -bigM*(1-b_betadown(cp,cs,l,ss))=l= sum{n,(-B(l,ss)»
    )*C(l,n)*theta(cp,cs,n,ss)}+ Fl(cp,cs,l,ss)-(1-nl(l,ss))*BigM;
523 e53(cp,cs,l,ss) .. sum{n,(-B(l,ss))*C(l,n)*theta(cp,cs,n,ss)}+ Fl(cp,c»
    s,l,ss)-(1-nl(l,ss))*BigM =l= bigM*(1-b_betadown(cp,cs,l,ss));
524 e54(cp,cs,l,ss) .. -bigM*(b_betadown(cp,cs,l,ss))=l=betadown(cp,cs,l,s»
   s);
525 e55(cp,cs,l,ss) ..
                            betadown(cp,cs,l,ss)=l=bigM*(b_betadown(cp,cs,l,ss)»
   );
526 e56(cp,cs,l,ss) ..
                            -bigM*(1-b_betaup(cp,cs,l,ss))=l= sum{n,B(l,ss)*C(l»
    ,n)*theta(cp,cs,n,ss) - Fl(cp,cs,l,ss)-(1-nl(l,ss))*BigM;
527 e57(cp,cs,l,ss) ..
                           sum{n,B(l,ss)*C(l,n)*theta(cp,cs,n,ss)}- Fl(cp,cs,l»
    ,ss)-(1-nl(l,ss))*BigM =l= bigM*(1-b_betaup(cp,cs,l,ss));
528 e58(cp,cs,l,ss) .. -bigM*(b_betaup(cp,cs,l,ss))=l=betaup(cp,cs,l,ss);
529 e59(cp,cs,l,ss) ..
                            betaup(cp,cs,l,ss)=l=biqM*(b_betaup(cp,cs,l,ss));
530 e68(cp,cs,l,ss) ..
                            -bigM*(1-b_alphadown(cp,cs,l,ss))=l= (-Fc(l,ss)*nl(»
    l,ss)*nc(l,ss)-Flc(cp,cs,l,ss));
531 e69(cp,cs,l,ss) ..
                             (-Fc(l,ss)*nl(l,ss)*nc(l,ss)-Flc(cp,cs,l,ss))=l= bi»
    gM*(1-b_alphadown(cp,cs,l,ss));
532 e70(cp,cs,l,ss) .. -bigM*(b_alphadown(cp,cs,l,ss))=l=alphadown(cp,cs,l»
   ,ss);
533 e71(cp,cs,l,ss) ..
                            alphadown(cp,cs,l,ss)=l=biqM*(b_alphadown(cp,cs,l,s»
   s));
534 e72(cp,cs,l,ss) ..
                            -bigM*(1-b_alphaup(cp,cs,l,ss))=l=(Flc(cp,cs,l,ss)-»
   Fc(l,ss)*nl(l,ss)*nc(l,ss));
535 e73(cp,cs,l,ss) ..
                            (Flc(cp,cs,l,ss)-Fc(l,ss)*nl(l,ss)*nc(l,ss))=l= big»
   M*(1-b_alphaup(cp,cs,l,ss));
536 e74(cp,cs,l,ss) ..
                           -bigM*(b_alphaup(cp,cs,l,ss))=l=alphaup(cp,cs,l,ss)»
    ;
537 e75(cp,cs,l,ss) ..
                           alphaup(cp,cs,l,ss)=l=bigM*(b_alphaup(cp,cs,l,ss));
538
539 e76(cp,cs,l,ss) ..
                           -biqM^*(1-b_epsilondown(cp,cs,l,ss)) = l = sum{n, (-B(l, *))}
   ss))*C(1,n)*thetac(cp,cs,n,ss)}+ Flc(cp,cs,1,ss)-(2-nl(1,ss)-nc(1,ss))*BiqM;
540 e77(cp,cs,l,ss) ..
                            sum{n, (-B(l,ss))*C(l,n)*thetac(cp,cs,n,ss)}+ Flc(cp»
    ,cs,l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM =l= bigM*(1-b_epsilondown(cp,cs,l,ss));
541 e78(cp,cs,l,ss) .. -bigM*(b_epsilondown(cp,cs,l,ss))=l=epsilondown(cp,»
   cs,1,ss);
542 e79(cp,cs,l,ss) ..
                            epsilondown(cp,cs,l,ss)=l=bigM*(b_epsilondown(cp,cs»
    ,l,ss));
543 e80(cp,cs,l,ss) ..
                            -bigM*(1-b_epsilonup(cp,cs,l,ss))=l= sum{n,B(l,ss)*»
   C(1,n)*thetac(cp,cs,n,ss)}- Flc(cp,cs,l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM;
544 e81(cp,cs,l,ss) ..
                            sum{n,B(l,ss)*C(l,n)*thetac(cp,cs,n,ss)}- Flc(cp,cs»
    ,l,ss)-(2-nl(l,ss)-nc(l,ss))*BigM =l= bigM*(1-b_epsilonup(cp,cs,l,ss));
545 e82(cp,cs,l,ss) ..
                            -bigM*(b_epsilonup(cp,cs,l,ss))=l=epsilonup(cp,cs,l»
    ,ss);
546 e83(cp,cs,l,ss) .. epsilonup(cp,cs,l,ss)=l= bigM*(b_epsilonup(cp,cs,l,»
   ss));
547 *
548 * These equations ensure that the selected strategy combination is a NE
549 *
550 Equation
551
      epi(cp,cs,ss)
552
553 ;
554 epi(cp,cs,ss)
                 ..
                            pi0(cp,ss)=q=pi(cp,cs,cp,ss);
555
556 Option rmip=cplex;
```

557
558 Model LinearNE /all/ ;
559
560 Solve LinearNE using rmip maximizing social\_cost ;
561
562